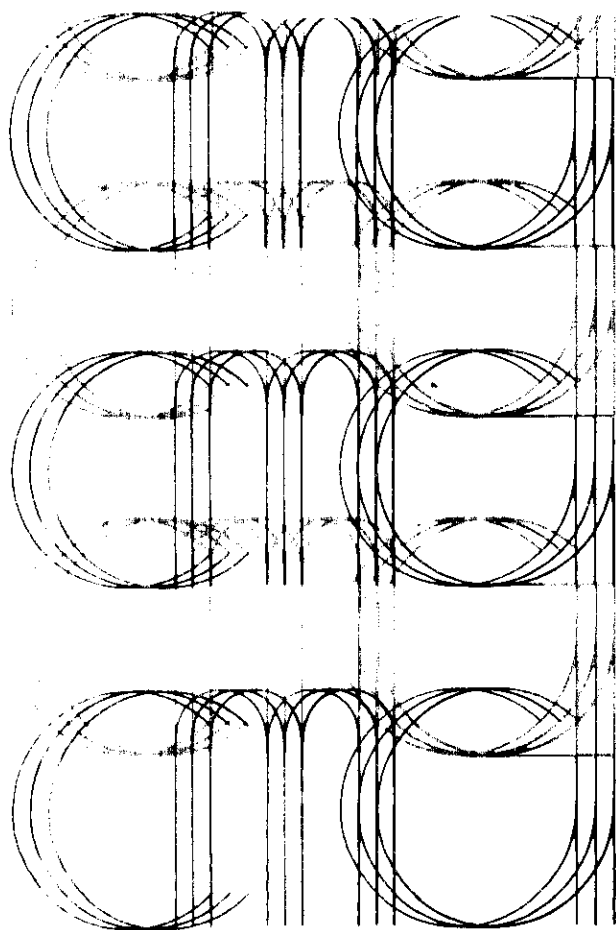
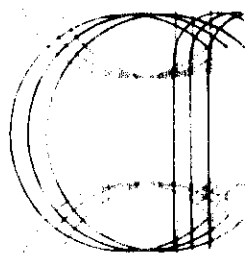


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COMPUTER MODELLING GROUP



**WASKADA MODEL STUDY
LOWER AMARANTH POOL**

for

OMEGA HYDROCARBONS LTD.

by

J. Flores and W. Laurila

May, 1983

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CALGARY, ALBERTA



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83-05-27

Mr. G.E. Patey
Vice-President Production
Omega Hydrocarbons Ltd.
630, 330 - 5 Avenue S.W.
Calgary, Alberta T2P 0L4

Dear Sir:

We are enclosing two copies of the Waskada model study which shows the model performance predictions for the Lower Amaranth Pool. The cases investigated the feasibility of gas injection and water flooding in a representative area of the field defined by four nine-spot patterns.

The three-dimensional, three phase Waskada mathematical model predicts good incremental recoveries if a secondary recovery scheme is implemented by October 1983. Specifically, based on a ten-year forecast gas injection results in an incremental recovery of 66.2 km^3 over the primary depletion case, whereas water flooding provides an incremental recovery of 59.4 km^3 . The recovery factors are 12.2, 20.1 and 19.3% model OOIP for the primary, gas injection and water flooding cases respectively. Extrapolated recoveries to an economic limit of $10 \text{ m}^3/\text{d}$ show expected ultimate recoveries of 12.2, 22.3 and 28.4% model OOIP indicating that ultimate recovery under water flooding is higher than recovery under gas injection.

It has been a pleasure to perform this reservoir model study for Omega. If you have any questions I shall be most happy to discuss it with you.

Yours truly,

J. Flores, Ph.D., P.Eng.
Manager - Applications

JF/cs

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SUMMARY

SUMMARY

This model study examines the feasibility of a secondary recovery scheme for the Waskada Field, Lower Amaranth Pool being developed by Omega Hydrocarbons Ltd.

Three cases were studied:

- . primary depletion;
- . gas injection;
- . water injection.

Results for the three cases are summarized below.

	<u>Primary</u>	<u>Gas Injection</u>	<u>Water Injection</u>
Recovery at ten years, %OOIP	12.2	20.1	19.3
Extrapolated Ultimate Recovery, % OOIP	12.2	22.3	28.4
Recovery at ten years, km ³	102.1	168.3	161.5
Extrapolated Ultimate Recovery, km ³	102.1	186.0	237.0
Peak Oil Rate, m ³ /d	64.1	74.0	68.0
Reservoir Life to Economic Limit, yrs.	10.0	11.8	15.0

All simulations were run using CMG's three phase, fully implicit, three dimensional black oil simulator BLAKO [1].

CONCLUSIONS

CONCLUSIONS

1. Due to the lack of supplied reservoir energy the reservoir pressure is declining at a dramatic rate of 1 250 kPa per year. At this rate of decline the reservoir pressure will reach the bubble point pressure of 4 220 kPa by June 1983.
2. Model predictions for a ten-year period show that gas injection will recover an additional 6.8 km³ of oil, giving an incremental recovery from 19.3 to 20.1% model OOIP over a water injection scheme. However, extrapolation to an economic limit of 10 m³/d indicates that the water flood ultimate recovery will be about 51 km³ higher than the gas injection giving an incremental recovery from 22.3 to 28.4% model OOIP.
3. Gas injection gives an incremental recovery of 66.2 km³ over the primary depletion case. This represents an increase in recovery factor from 12.2 to 20.1% model OOIP based on a ten-year forecast.
4. To carry out a gas injection scheme, a total of 7 350 km³ of make-up gas will be required for each portion of the field equal to the study area (four nine-spot patterns). The average rate of make-up gas requirement is 5.76 km³/d over three and a half years.
5. Water injection gives an incremental recovery of 59.4 km³ over the primary depletion case. This represents an increase in recovery factor from 12.2 to 19.3% model OOIP based on a ten-year forecast.

RECOMMENDATIONS

RECOMMENDATIONS

1. A secondary recovery project should be implemented as soon as possible in the Waskada Lower Amaranth Pool to eliminate the critical reservoir pressure decline observed in the field and predicted by the reservoir model.
2. Although model predictions show the highest ultimate recovery under water flooding, the final scheme to be implemented has to be defined based on the relative economics of water injection vs gas injection. A gas injection scheme has a good potential for recovering additional hydrocarbon liquids through mass transfer between the injection gas and the reservoir oil.
3. To increase the reliability of model predictions with regard to the level of absolute recoveries, an update model study is recommended when more reservoir rock data and production history from additional development wells become available. At that time a three dimensional compositional model study may be required to predict total hydrocarbon liquids recovery including those recovered from the separator gas.
4. Gas availability in the area should be investigated to examine the feasibility of a fieldwide gas injection project. If not enough gas is available, some patterns could be converted to water flood after a period of gas injection. A model study may be necessary to examine the performance of gas injection for a certain period followed by water flooding.
5. The set of fluid distribution curves developed as part of this study (Appendix B) should be used to determine more accurately the water saturation profile in the Waskada Lower Amaranth Pool.

DISCUSSION

DISCUSSION

MODEL DEVELOPMENT

The location of the Waskada Field, shown in Figure 1, is approximately one hundred and ten kilometers southwest of Brandon, Manitoba in Township 1, Ranges 25 and 26 and Township 2, Ranges 25 and 26. The model study area is restricted to Township 1, Range 25, Sections 30 and 31 and Township 1, Range 26, Sections 25 and 36. This study area includes four nine-spot patterns with each pattern having one injector. Details on the development of the Waskada three-dimensional, three phase mathematical model is presented in Appendix A.

Reservoir Description and Fluid Properties

Data from the Waskada Field indicated that the reservoir to be modelled was very heterogeneous with wide variations in net pay, porosity and permeability. The reservoir fluid is an undersaturated low viscosity oil. The reservoir pressure is about 4 400 kPa higher than the bubble point pressure.

Field Geology

The Waskada Lower Amaranth sand is at a depth of about 900 m KB. The traps are controlled by pinchouts of porosity and permeability in all directions. The sand is usually poorly developed with porosities and permeabilities uniformly low. The sand contains abundant thinly interbedded tight stringers. There is no gas-oil contact and the oil-water contact is currently estimated at 465 m subsea. The sand dips very gently in a southerly direction and the hydrocarbon traps occur independently of the structure. A typical log from the 13-30-1-25 W1M well is shown in Figure 2.

Reservoir Rock Data

Net pay values in the Lower Amaranth Pool (study area) vary from 3 to 12 m and depths to the top of the sand from 425 to 438 m subsea. Porosity values range from 2 to 20%, with an average of 13% and permeability values from .02 to 100 mD with most common values in the range of 0.5 to 10 mD. Computer generated contour maps for depth, net pay and porosity corresponding to the four pseudo layers in the model are presented in Figures A-2 through A-10.

Permeability values for each grid block in the model were calculated using a functional relationship between permeability and porosity as indicated in Figure A-11. Tables A-1 through A-6 show the reservoir rock input data for the three-dimensional model.

An average capillary pressure curve corresponding to a permeability of 3.7 mD and a porosity of 13% was used in the model. This resulted in an irreducible water saturation of 44%. Figure A-12 shows the average oil-water capillary pressure curve. The gas-oil capillary pressure was input as zero.

Data from five core samples were used to determine the average capillary pressure curve that would give a water saturation profile consistent with water saturations seen in a special core obtained with an oil base drilling fluid [2]. The average water saturation was about 63%.

Due to the high degree of heterogeneity observed in the Waskada Lower Amaranth Pool, a set of fluid distribution curves was developed to provide an accurate estimate of the expected water saturation levels for new wells. The development of the fluid distribution curves and a procedure to calculate the water saturation profile is presented in Appendix B.

Average sets of oil-water and gas-oil relative permeabilities were obtained using the available relative permeability data [2]. Figures A-13 and A-14 in Appendix A show the representative curves after slight adjustments performed for consistency with capillary pressure data and for improvement of history match. A three phase oil relative permeability was calculated using Stone's equation which combines data from the two-phase systems, i.e. oil-water and gas-oil.

The model can be rapidly updated as new field data becomes available. This is done through a set of FORTRAN routines written in conjunction with a surface graphics package [3].

Fluid Properties

The Waskada Lower Amaranth Pool is an undersaturated hydrocarbon system having a bubble point pressure of 4 220 kPa at a reservoir temperature of 45.0°C. This bubble point pressure is about 4 400 kPa lower than the initial reservoir pressure of 8 672 kPa.

Reservoir oil viscosities vary from a minimum of about 1.3 mPa·s at the bubble point pressure to a maximum of 2.9 mPa·s at atmospheric pressure. Initial solution gas-oil ratio is 51.1 m³/m³. Water, oil and rock compressibilities used in the model are 4.4×10^{-7} kPa⁻¹, 1.2×10^{-6} kPa⁻¹, and 6.7×10^{-7} kPa⁻¹, respectively.

Table A-10, "PVT Functions", outlines the reservoir fluid properties obtained from a PVT study [4].

Grid System and Well Locations

The grid system consists of four slices (A,B,C,D) corresponding to the four pseudo layers to model the Lower Amaranth Pool. A 15 by 15 areal configuration (Figure A-1) gives a total of 900 grid blocks.

A set of twenty five-well locations (Figure A-1) in Township 1, Range 25, Sections 30 and 31 and Township 1, Range 26, Section 25 and 36 were selected to model the behaviour of a symmetric pattern in the field. One of the quarter wells (9-36-1-26 W1M) did not find the Lower Amaranth Pool and therefore was removed from the model. The symmetric pattern incorporates fifteen and three quarters effective wells.

Initial Conditions

The following are the initial conditions for the study area:

Reservoir Pore Volume	:	3 370 km ³
Original Oil-In-Place	:	836.1 km ³
Original Gas-In-Place (solution gas)	:	42 900 km ³
Original Water-In-Place	:	2 310 km ³

Initial conditions are calculated automatically using the gravity-capillary equilibrium feature of the simulator. Reservoir pressure, oil saturation and water saturation distributions are shown in Tables A-7, A-8 and A-9 respectively. The initial reservoir pressure of 8 620 kPa at a datum of 420 m subsea was obtained from a build-up test 5 .

History Matching

A satisfactory match was obtained for the overall twenty four-well locations in the model. Due to somewhat erratic field production data available at this early stage in the field development, no additional runs were done to refine the match of production history and flowing bottomhole pressures on a well by well basis. Details to carry out the history match are presented in Appendix B.

After obtaining a satisfactory history match the model was used to predict reservoir performance under primary depletion, gas injection and water injection. Analysis of these predictions are discussed next.

ANALYSIS OF MODEL PREDICTIONS

Model predictions show that implementation of a secondary recovery scheme by injecting gas or water will approximately double the predicted oil recovery under primary depletion. The highest ultimate recovery under water injection (extrapolated value) amounts to 28.4 % OOIP. This compares with an ultimate recovery of 22.3% under gas injection. Recoveries for the ten-year forecasts, however, show gas injection giving a recovery of 20.1% OOIP which compares with the lower recovery of 19.3% under water injection.

Figure 3 and Table 1 show the recoveries obtained at the end of a ten-year forecast and the expected ultimate recoveries at an economic limit of 10 m³/d. Predicted oil production rate forecasts for primary depletion, gas injection and water injection are presented in Table 2. In all three cases the limiting flowing bottom hole pressure was 500 kPa.

Model predictions also show a very high rate of reservoir pressure decline during primary depletion due to lack of supplied reservoir energy. Under the current expected production rates the bubble point pressure of 4 220 kPa will be reached by June 1983.

At the end of the production history matching in November 1982, some sequential development was simulated during 1983 and 1984. The number of effective wells in the symmetric pattern increased from 9 to a total of 15 3/4 wells. Table A-11 in Appendix A shows the wells on production during the history match and the expected sequential

development until October 1984. Gas or water injection commenced in October 1983 with injectors defined by the 5-31, 7-31, 13-30 and 15-30 wells corresponding to the four nine-spot patterns in the study area.

Recoveries

Figure 3, "Percentage Recovery Original Oil-in-Place vs Percentage Expected Ultimate Recovery", shows the long term highest recovery of the water injection case over both the gas injection and the primary depletion cases. Using an economic limit of 10 m³/d the extrapolated expected ultimate recoveries for primary depletion, gas injection and water injection are 12.2, 22.3 and 28.4% OOIP, respectively. Remaining oil saturations for the three cases are shown in Tables A-15, A-18, and A-19.

Figure 3 shows that at the end of ten years the oil recovery under water injection is only about 70% of its expected ultimate recovery, whereas under gas injection the recovery is about 90% of its expected ultimate recovery. The reservoir life to produce the ultimate reserves under gas injection is estimated at 11.8 years and for water injection is estimated at 15 years. The corresponding predicted recoveries at the end of a ten-year forecast are: 12.2, 20.1 and 19.3% OOIP. Reservoir performance predictions are summarized in Tables 3 to 5 and recoveries for the individual wells are summarized in Table A-12.

Oil Rate

Figures 4, 5 and 6 graph oil rate vs time, vs cumulative oil production and vs percentage expected ten year recovery, respectively. Gas injection gives the maximum oil rate of 74 m³/d after six and a half years when cumulative production is about 94 km³, representing 52% of the ten year expected recovery. During the first six and a half years of gas or water injection, it is seen that the water injection case predicts lower oil rates

than the gas injection case due to high water saturation levels. However after this period, due to high gas-oil ratio, the oil rate decline under gas injection is much faster than the decline observed under water injection. This results in a higher ultimate recovery for water flooding when extrapolated to an economic limit of 10 m³/d.

Gas-Oil Ratio Performance

As observed in Figure 7, "Instantaneous Producing Gas-Oil Ratio vs Time", gas injection causes the producing GOR to continuously increase with time to 2 000 m³/m³ at the end of ten years. Water injection, effectively controlled the producing GOR bringing it down to levels corresponding to the initial solution GOR.

Also, gas injection causes substantial increase in gas production to a maximum of about 102 km³/d after nine years of production (Fig. 8). Under water injection the maximum gas production rate is only about 5 000 m³/d which is lower than the maximum gas rate of approximately 10 000 m³/d predicted under primary depletion.

Water-Cut Performance

Figure 9, "Instantaneous Water Cut vs Time", shows water cut levels ranging from 40% to 72%, peaking at 72% for the water injection case at the end of the tenth year.

In Figure 10, "Instantaneous Water Production Rate vs Time", it is seen that water production increases substantially in the water injection case and peaks at 120 m³/d at the end of ten years. Under gas injection, the water production rate is approximately constant at an average of about 55 m³/d. Under primary depletion due to loss in well productivity and due to solution gas expansion the water production peaks only at 50 m³/d in June 1984 and continuously decreases to a minimum of about 15 m³/d at the end of ten years.

Gas Injection Case - Gas Production and Injection Rates

Figure 11, "Gas Production and Injection Rates vs Time", shows that make-up gas in the amount of 7 350 km³ is required to increase the reservoir pressure to an average of 6 000 kPa. The average make-up gas rate was 5.76 km³/d for a period of three and a half years. Thereafter, only the separator gas production is put back into the reservoir to maintain the reservoir pressure at an average of about 5 000 kPa. The peak gas injection rate was 102 km³ after nine years of production. The gas injection rates in this study were developed without considering the reduction in gas volumes that will occur due to fuel requirements and liquid shrinkage. The remaining gas-in-place (free plus solution gas) at the end of the ten-year forecast is about 49 Mm³.

The reservoir pressure response to fluid injection is discussed under the Reservoir Pressure section.

Water Injection Case - Water Production and Injection Rates

A maximum water injection rate of 240 m³/d for a period of three months brought the average reservoir pressure to a level of about 6 000 kPa. This increase in reservoir pressure is achieved in approximately three months. After this period, the water injection rate was reduced to an average of 150 m³/d to maintain the reservoir pressure at about 5 000 kPa.

The reservoir pressure response under fluid injection is discussed below.

Reservoir Pressure

Figures 13, 14 and 15 show reservoir pressure vs time, vs cumulative oil production, and vs percentage expected ten-year recovery, respectively.

Due to lack of external reservoir energy; the rate of reservoir pressure decline under primary depletion is extremely high and amounts to 1 250 kPa/yr (Figure 13). Under primary depletion, the average reservoir pressure will reach the bubble point pressure of 4 220 kPa by June 1983. At this time the cumulative oil production is about 9 km³ (Figure 14) equivalent to approximately 8% of the primary reserves in the model (Figure 15).

The figures show that water injection more effectively replaces fluid withdrawals from the reservoir. With water injection the maximum pressure level of 6 000 kPa is obtained after three months of injection when 20% of the reserves has been produced. With gas injection, however, the same pressure level is obtained after three and a half years of injection when 50% of the reserves under gas injection is produced (Figure 15).

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3. Sampson, R.J., "Surface II Graphics System", Revision 1, Kansas Geological Survey, Lawrence, Kansas (1978).
4. Core Laboratories Canada Ltd., "Reservoir Fluid Study", Report 7013-82-20, (April 19, 1982).
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FIGURES

Figure 1
LOCATION OF THE WASKADA FIELD

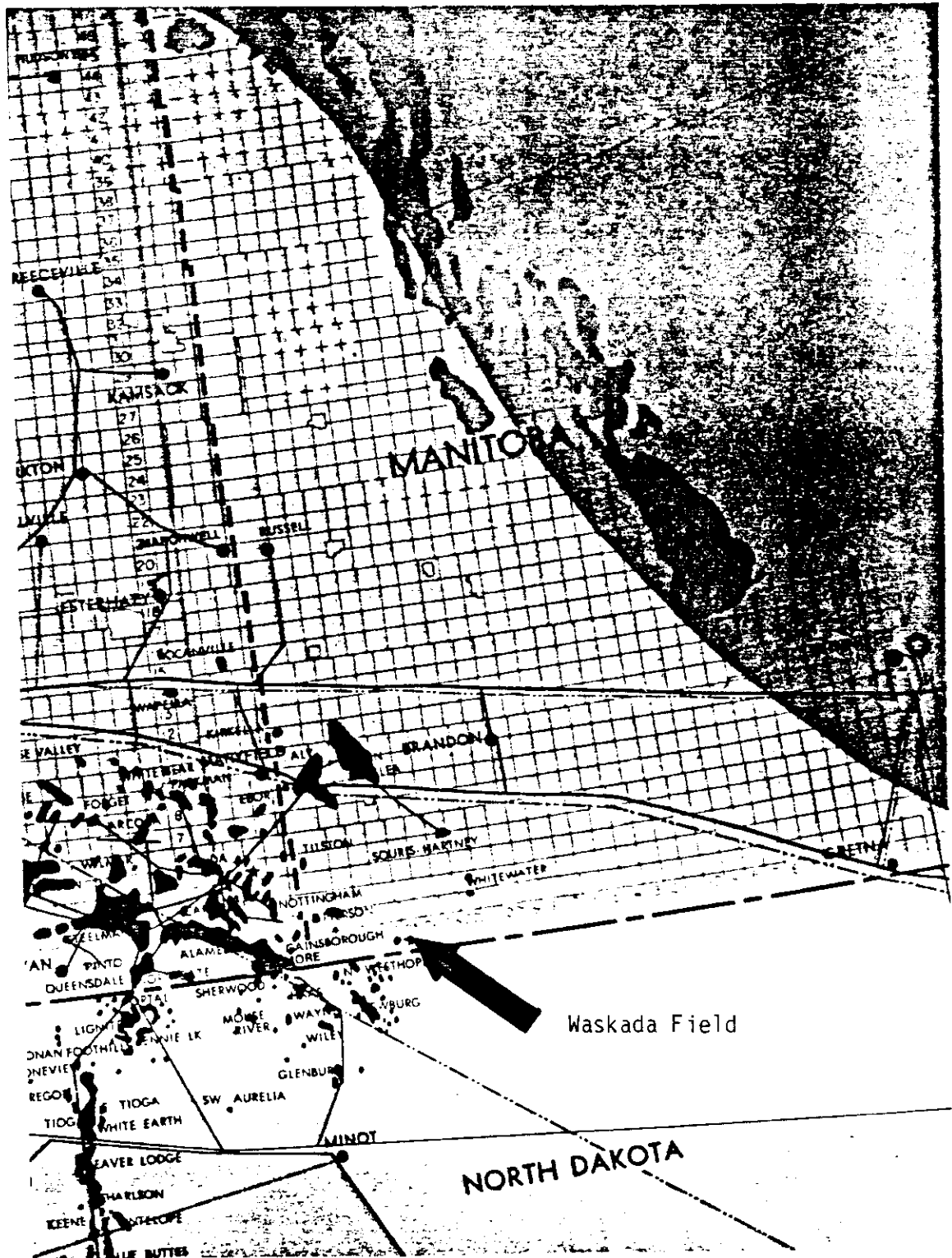


Figure 2

TYPICAL WELL LOG

13-30-1-25 W1M

Waskada Lower Amaranth Pool

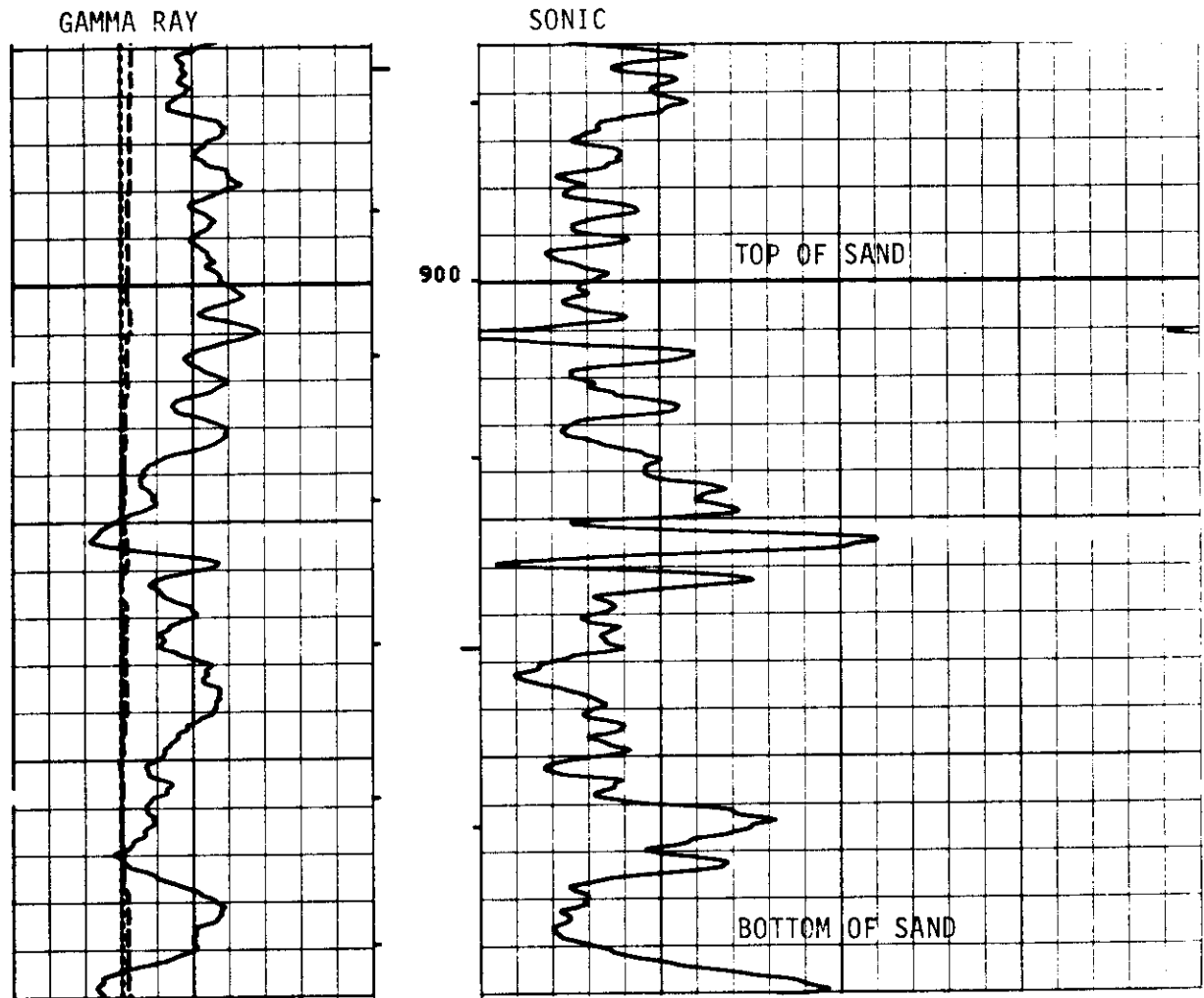


Figure 3
% RECOVERY OOIP VS % EXPECTED ULTIMATE RECOVERY
WASKADA LOWER AMARANTH POOL

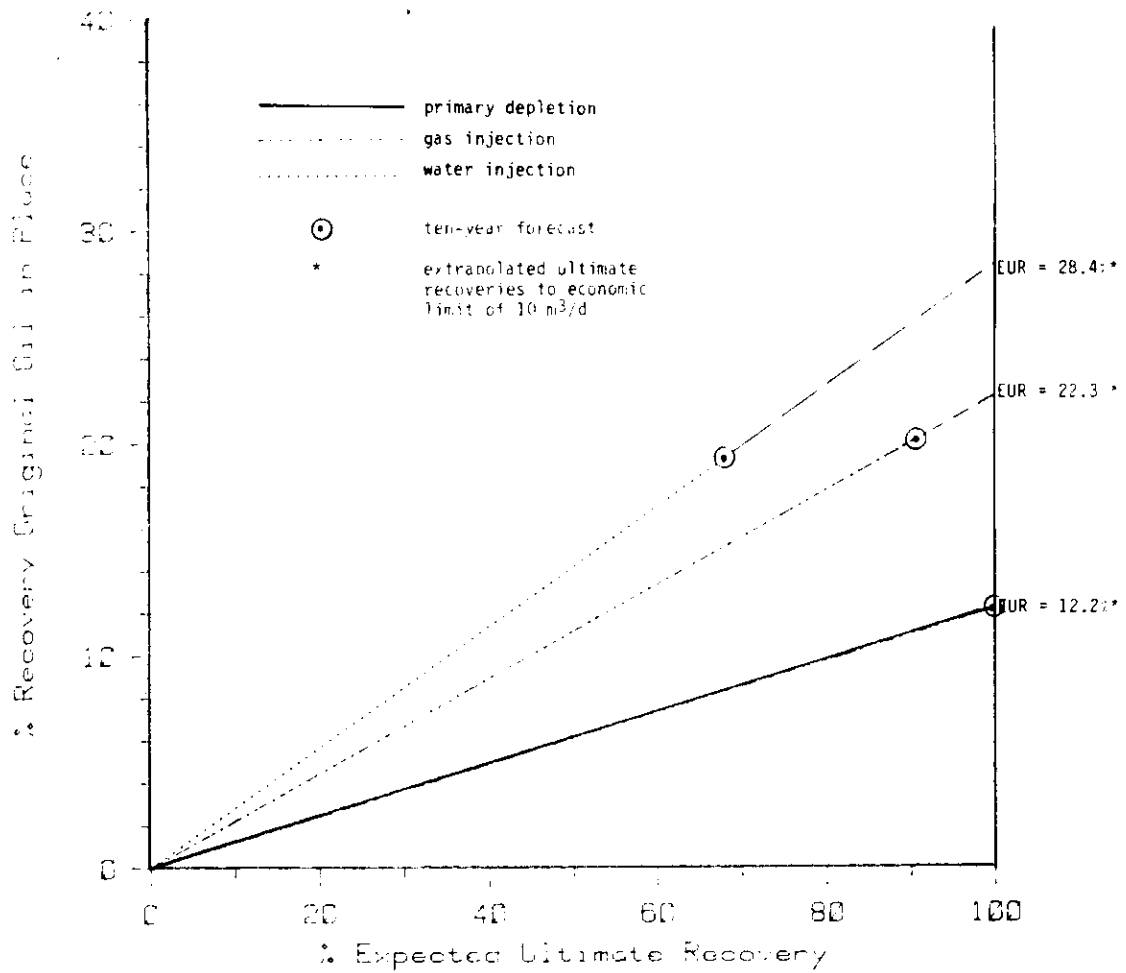


Figure 4
INSTANTANEOUS OIL PRODUCTION RATE VS TIME
Waskada Lower Amaranth Pool

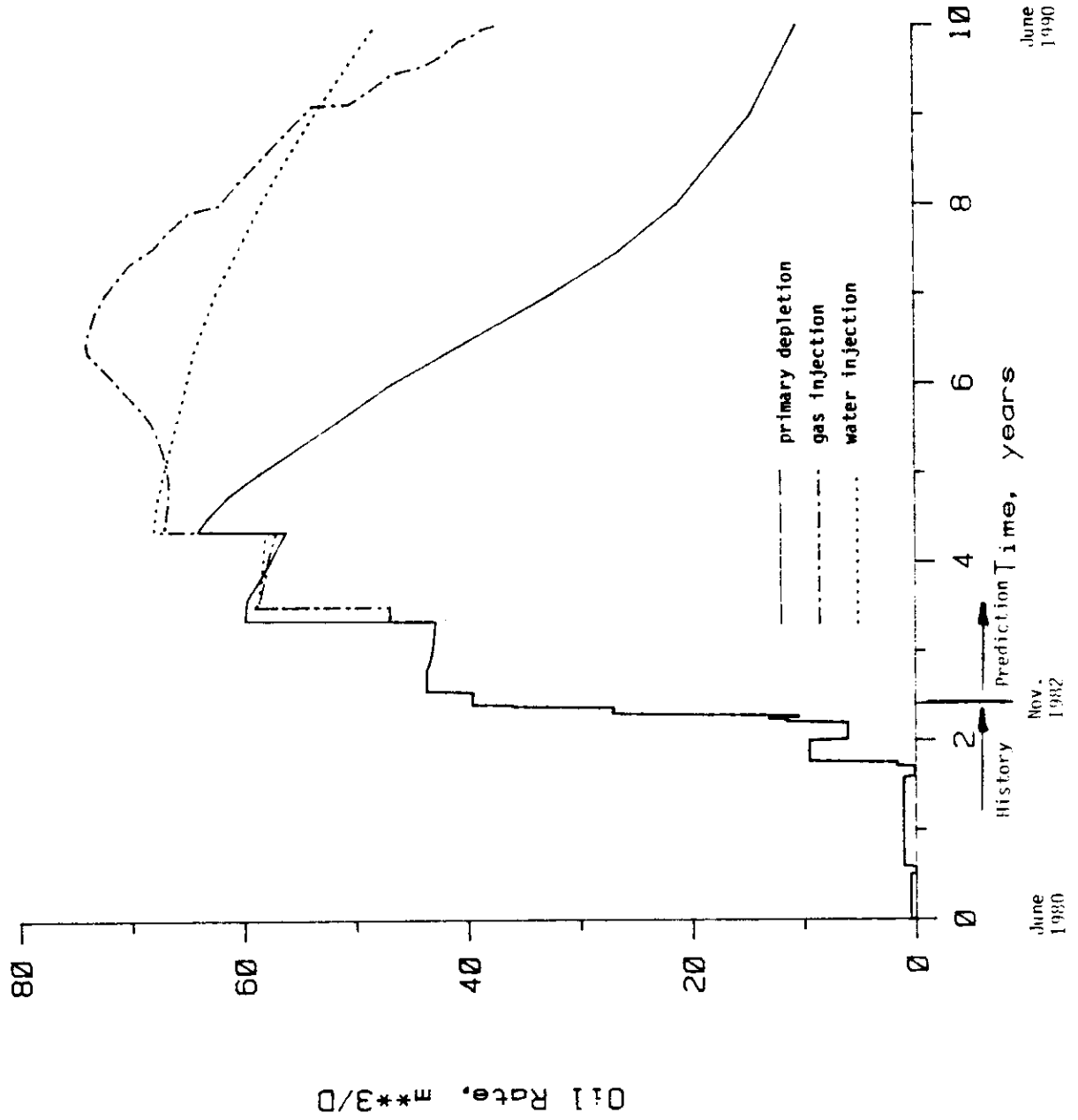


Figure 5
INSTANTANEOUS OIL RATE VS CUMULATIVE OIL PRODUCTION
Waskada Lower Amaranth Pool

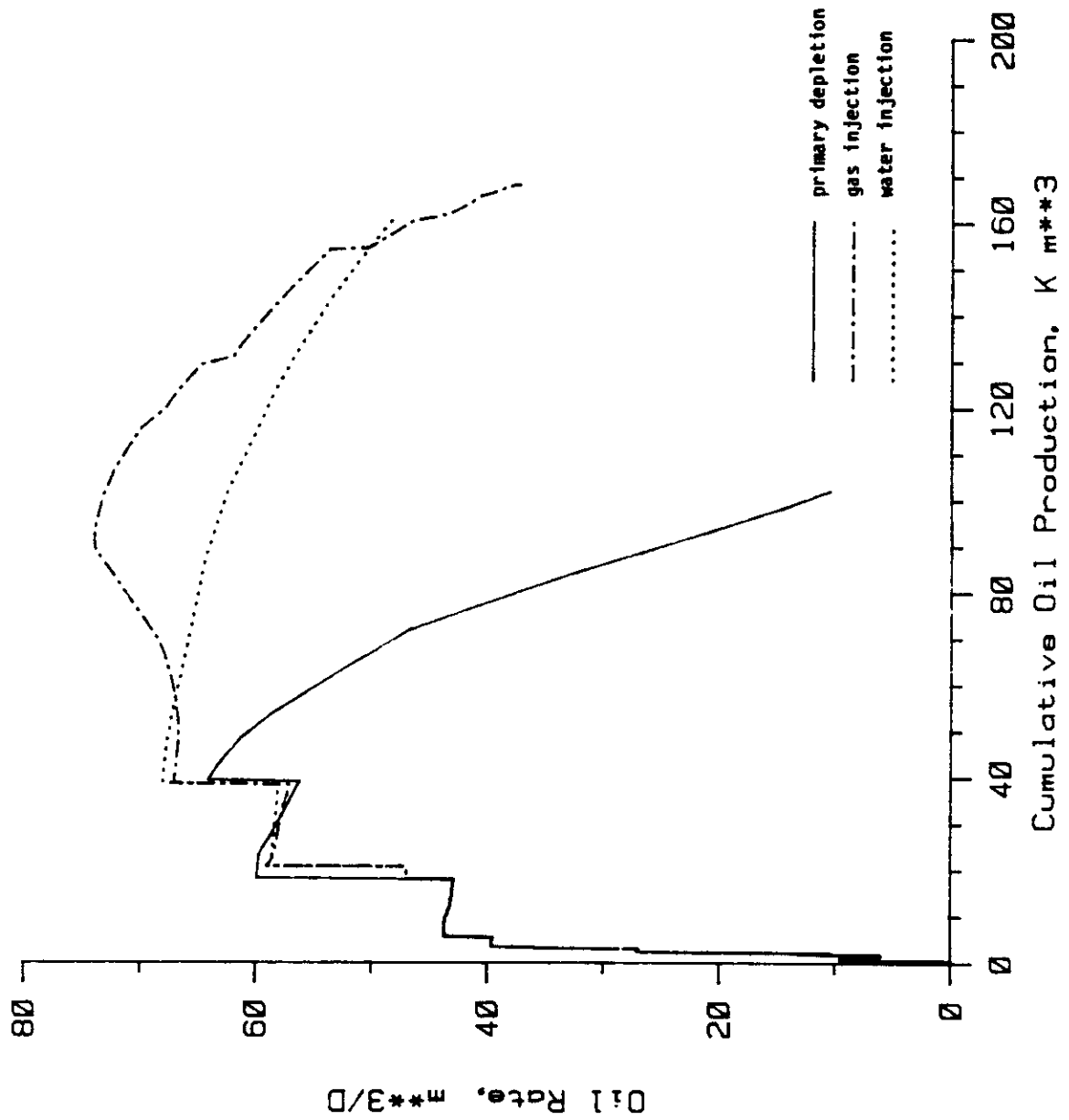


Figure 6
OIL RATE VS % EXPECTED TEN-YEAR RECOVERY
Waskada Lower Amaranth Pool

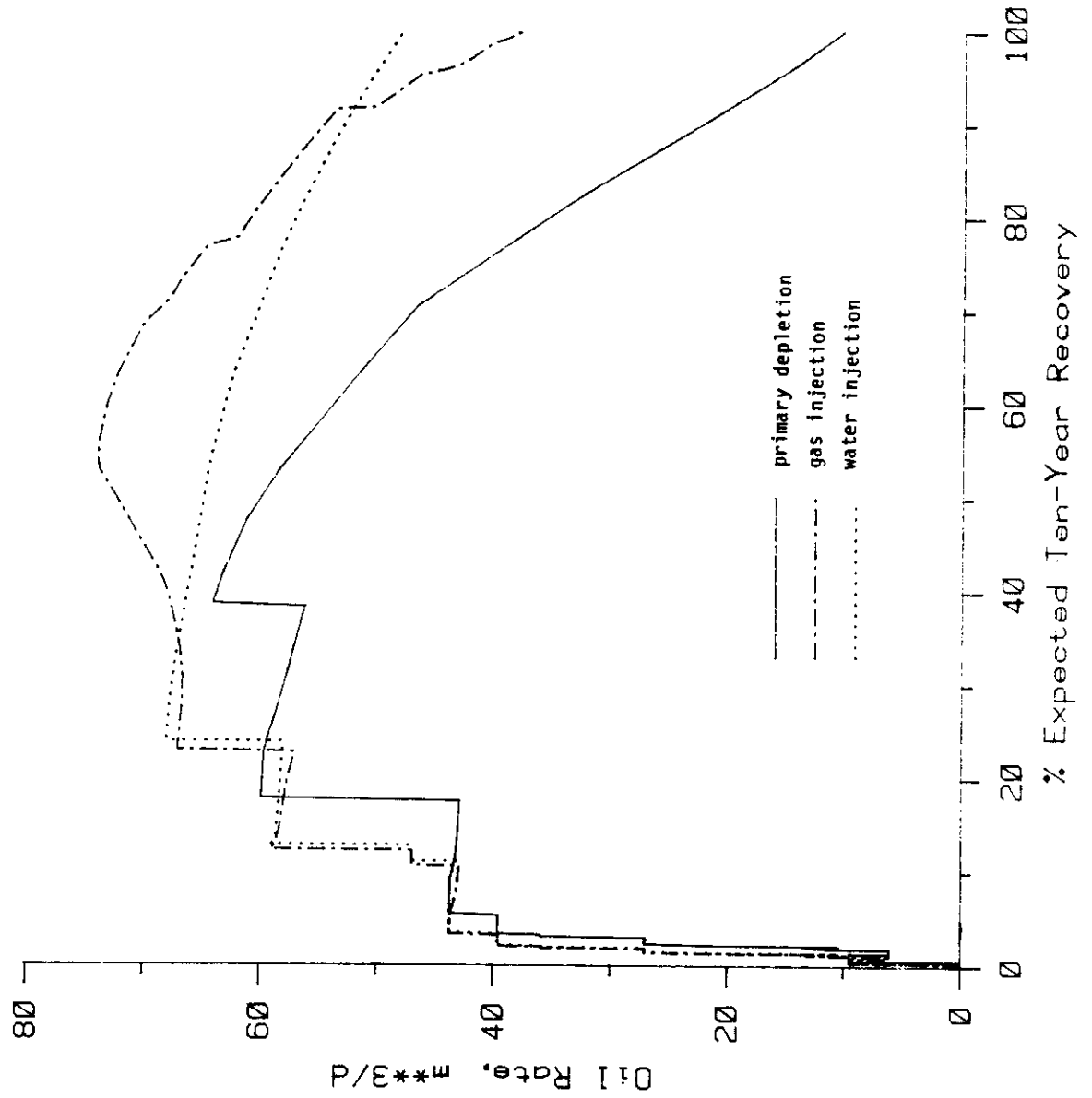


Figure 7
INSTANTANEOUS PRODUCING GAS OIL RATIO VS TIME
Waskada Lower Amaranth Pool

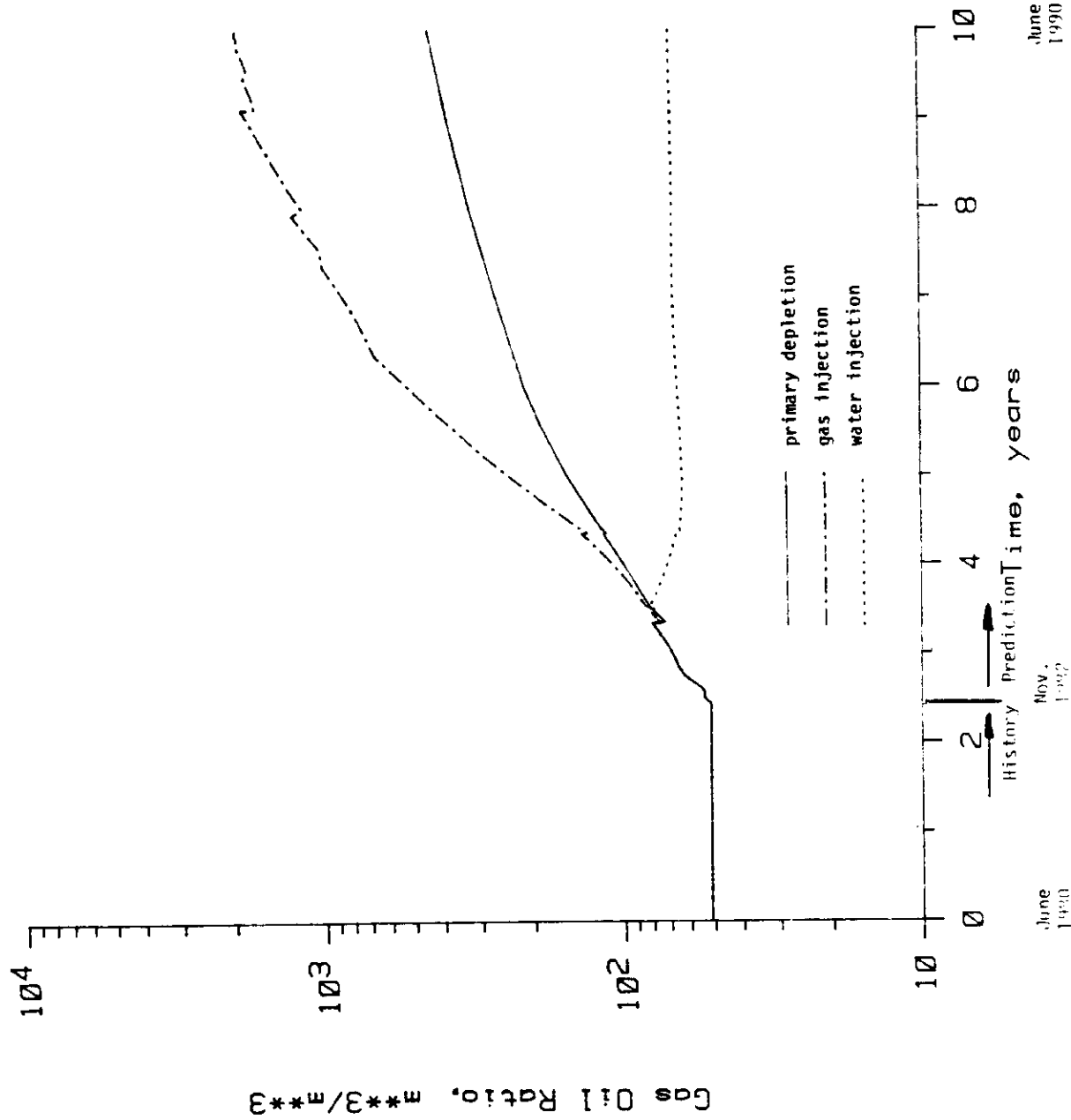


Figure 8
INSTANTANEOUS GAS PRODUCTION RATE VS TIME
Waskada Lower Amaranth Pool

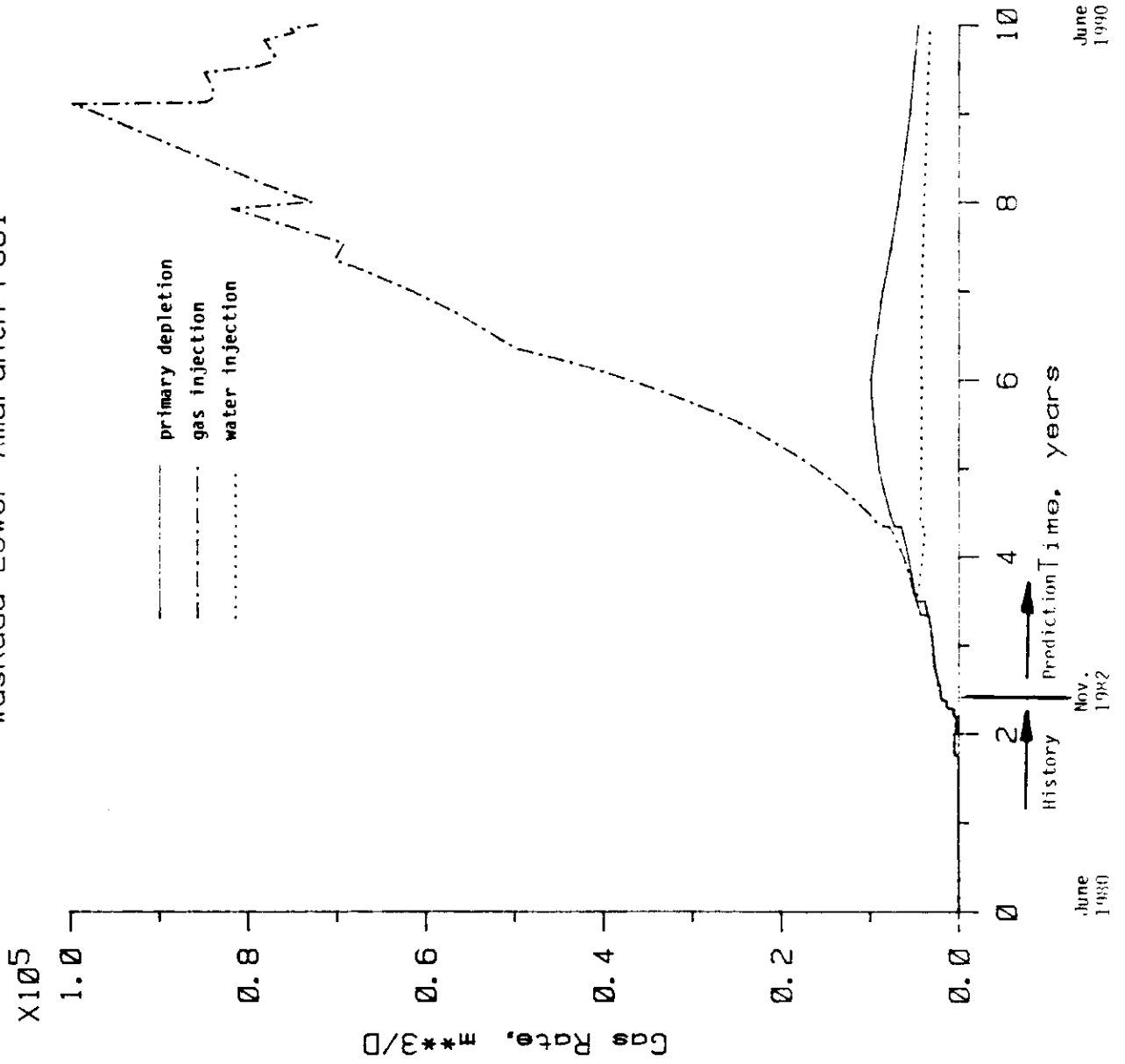


Figure 9
INSTANTANEOUS WATER CUT VS TIME
Waskada Lower Amaranth Pool

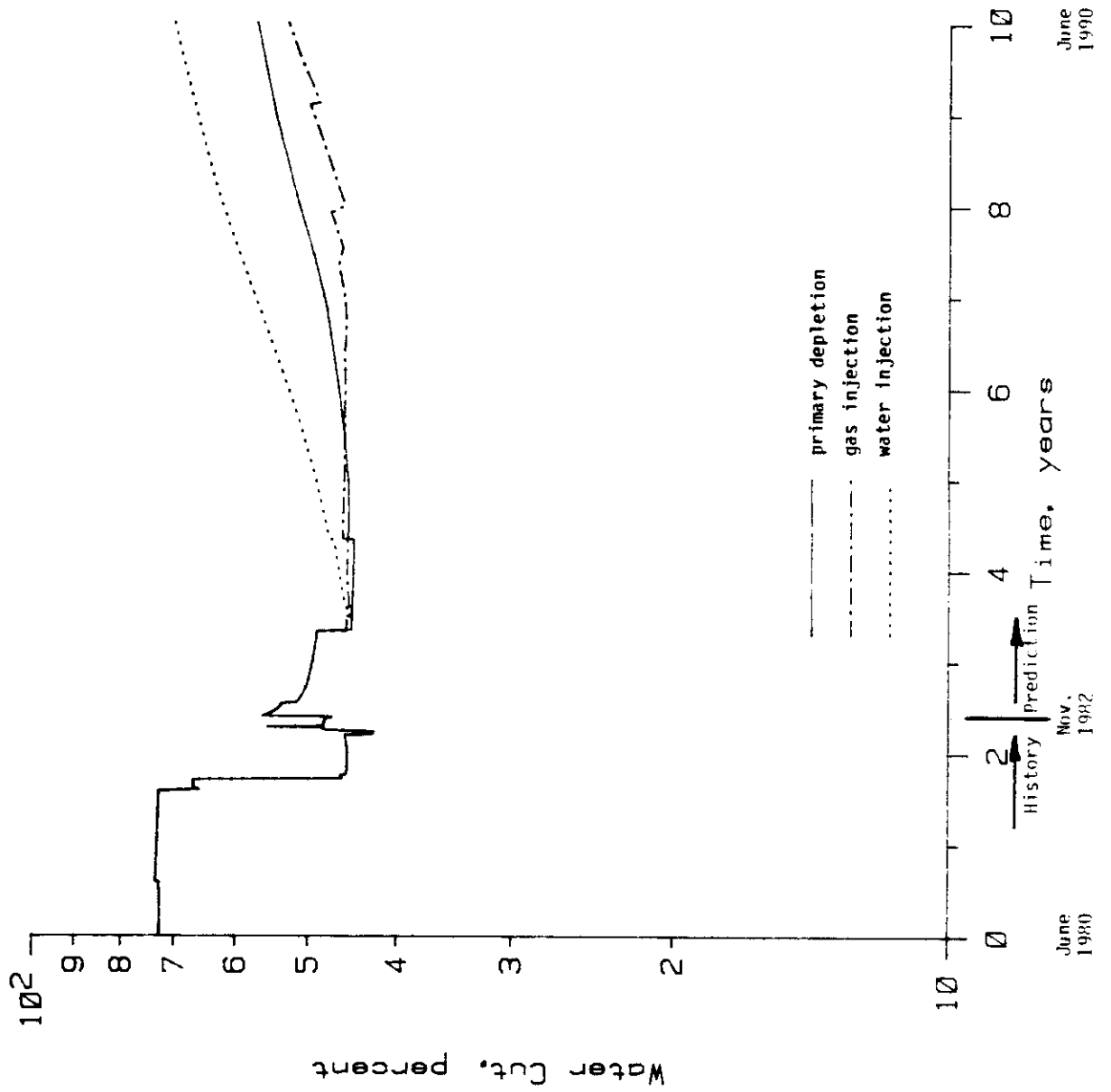


Figure 10
INSTANTANEOUS WATER PRODUCTION RATE VS TIME
Waskada Lower Amaranth Pool

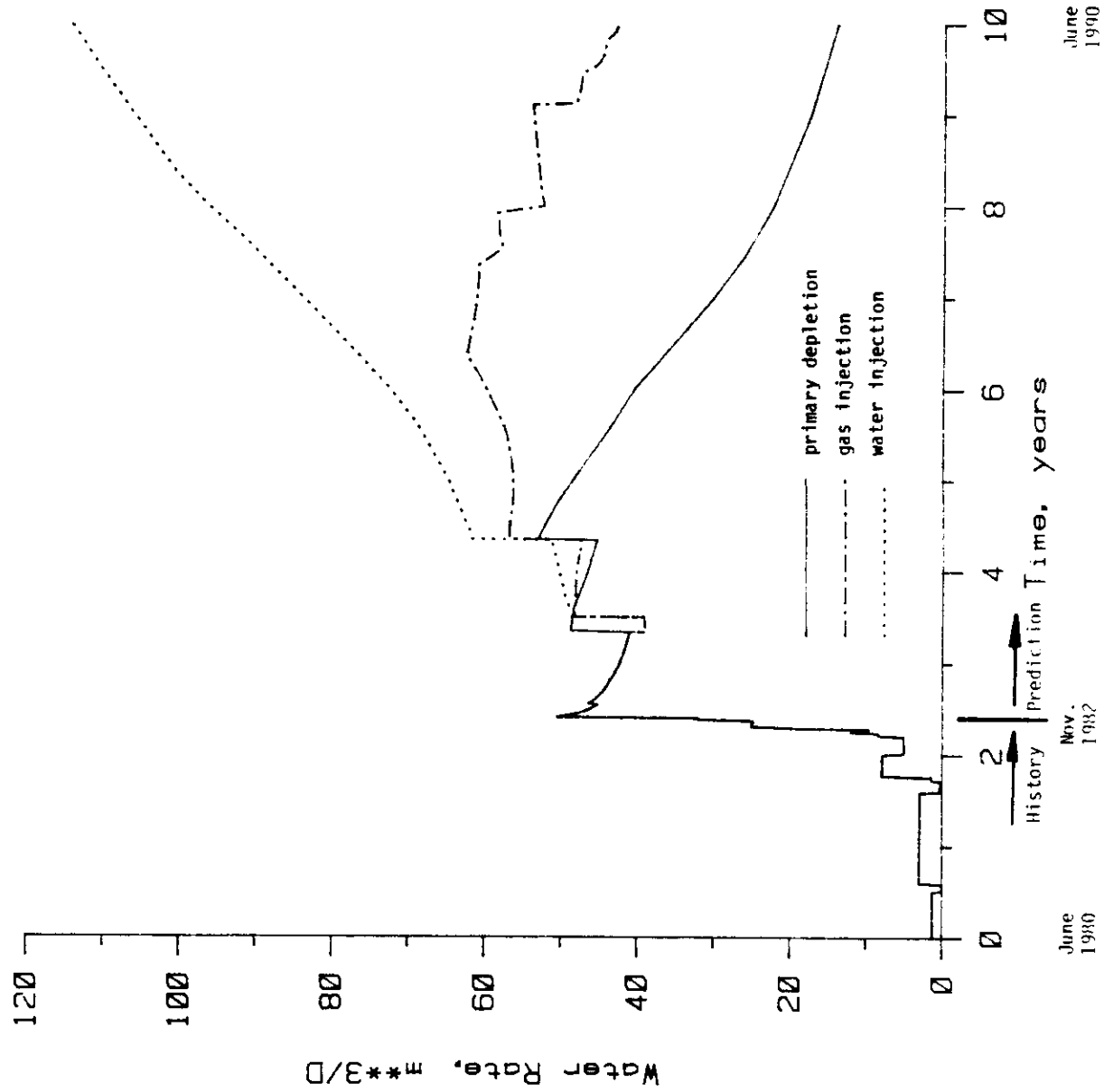


Figure 11
GAS PRODUCTION AND INJECTION RATES VS TIME
Waskada Lower Amaranth Pool

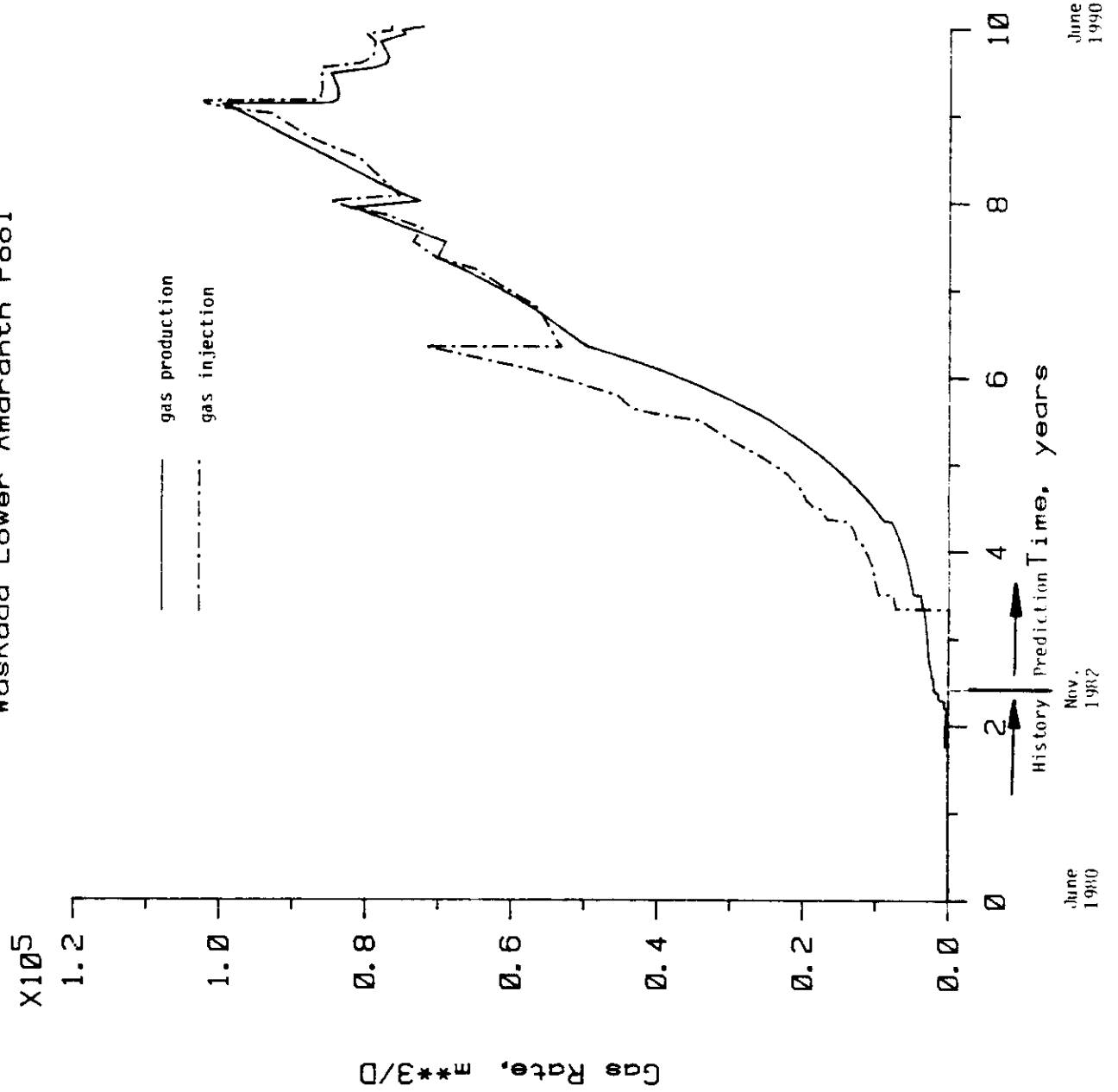


Figure 12
WATER PRODUCTION AND INJECTION RATES VS TIME
Waskada Lower Amaranth Pool

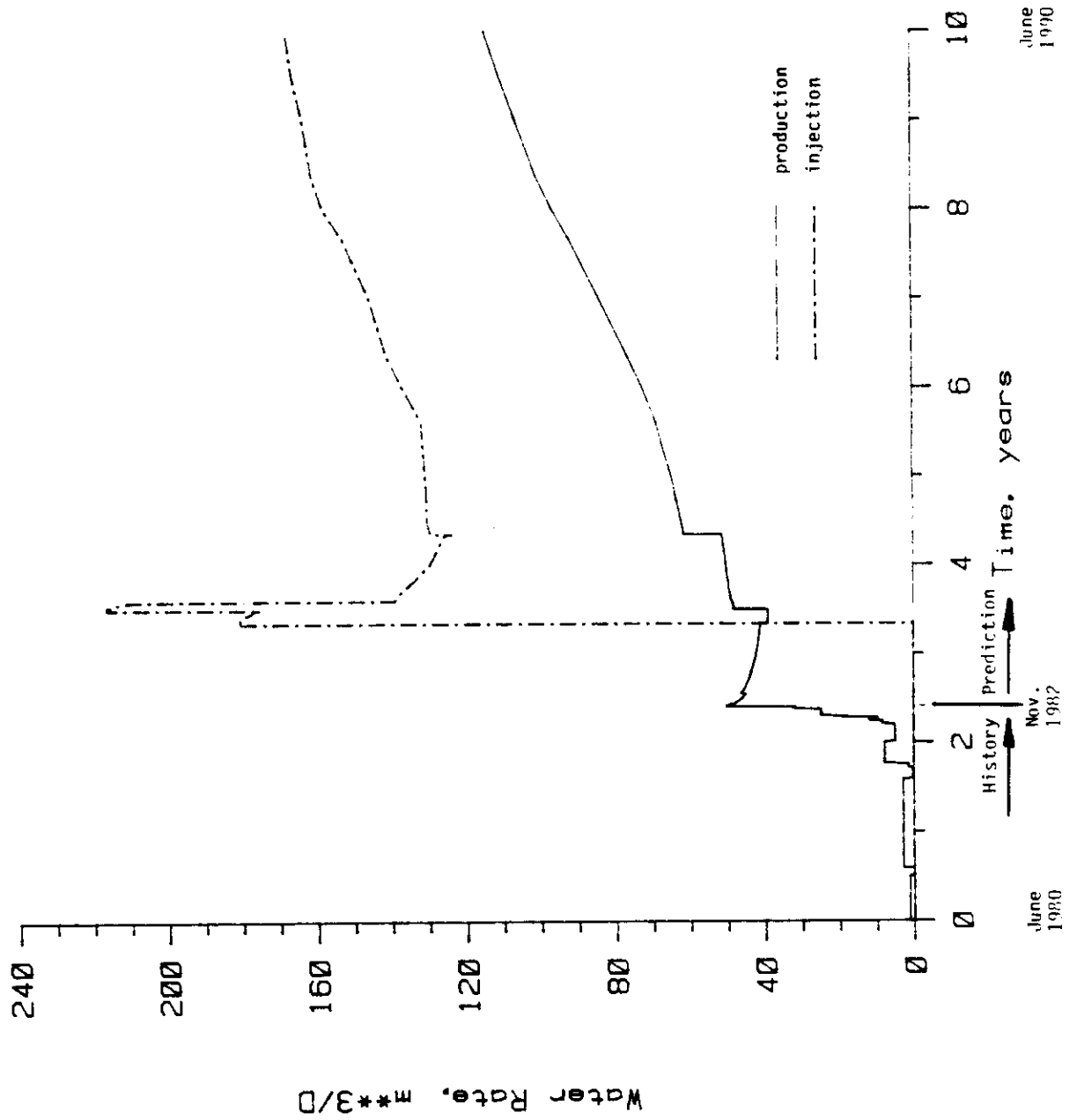


Figure 13
RESERVOIR PRESSURE DECLINE
Waskada Lower Amaranth Pool

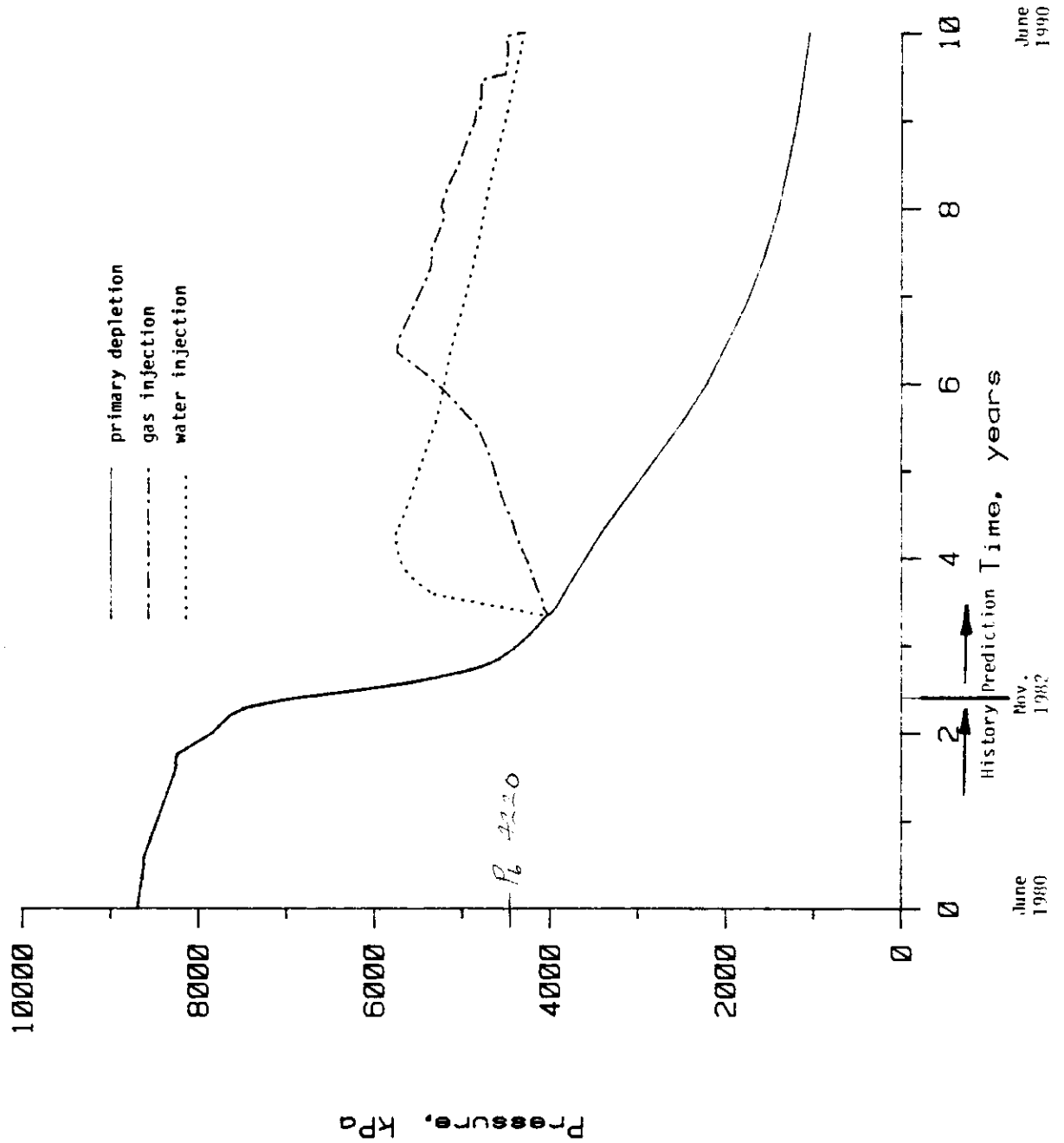


Figure 14

RESERVOIR PRESSURE VS CUMULATIVE OIL PRODUCTION

Waskada Lower Amaranth Pool

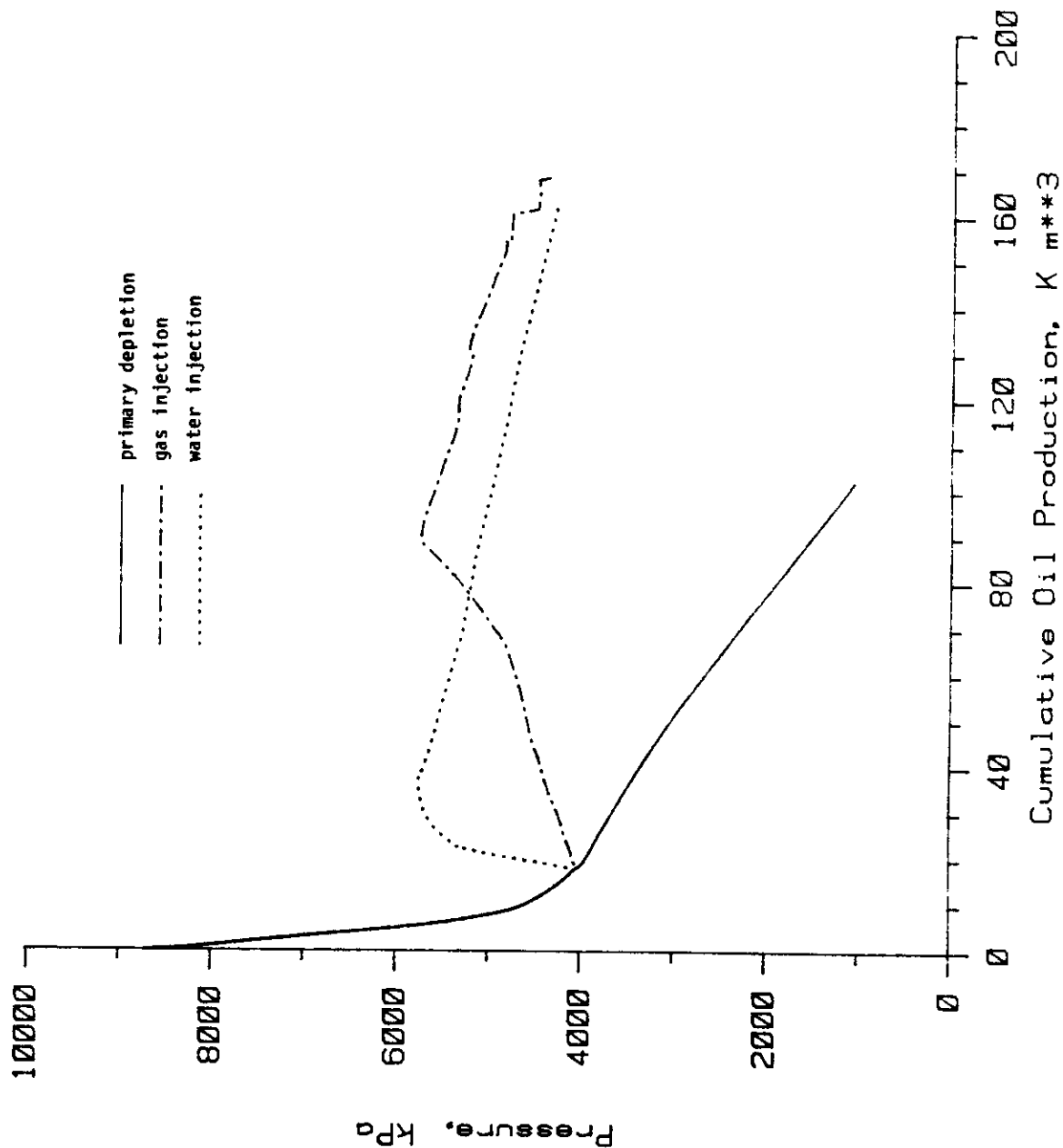
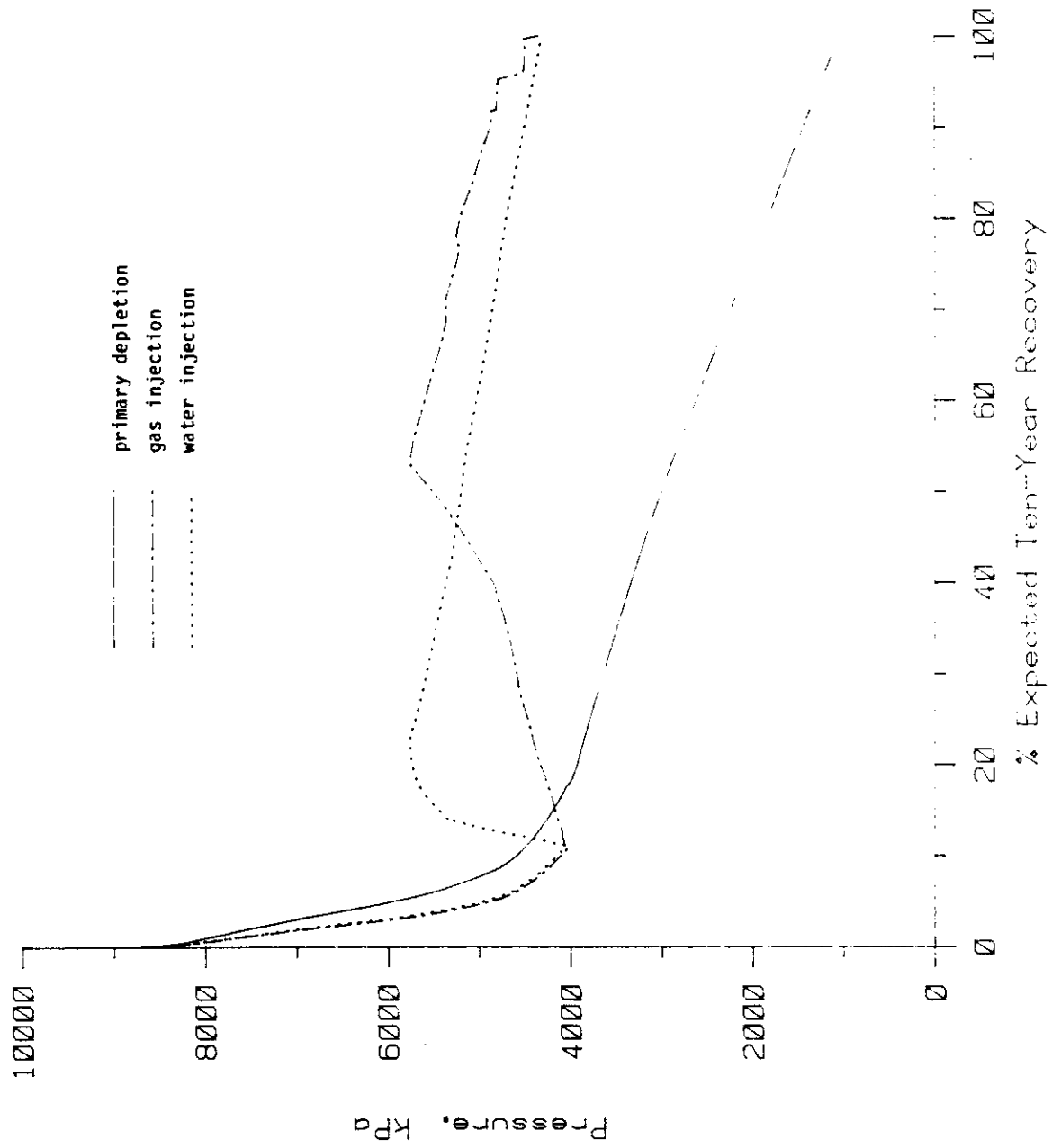


Figure 15
RESERVOIR PRESSURE VS % EXPECTED TEN-YEAR RECOVERY
Waskada Lower Amaranth Pool



TABLES

Table 1

SUMMARY OF RECOVERIES

Waskada Lower Amaranth Pool

<u>Case</u>	<u>10 Year Forecast</u>		<u>Economic Limit of 10 m³/d</u>	
	<u>km³</u>	<u>% Model OOIP</u>	<u>km³</u>	<u>% Model OOIP</u>
Primary Depletion	102.1	12.2	102.1	12.2
Gas Injection	168.3	20.1	186.0	22.3
Water Injection	161.5	19.3	237.0	28.4

Table 2
SUMMARY OF OIL PRODUCTION RATE FORECASTS

Waskada Lower Amaranth Pool

Year	Primary Depletion		Gas Injection		Water Injection	
	Rate, m ³ /d	Cum. Oil km ³	Rate, m ³ /d	Cum. Oil km ³	Rate, m ³ /d	Cum. Oil km ³
1980	0.41	.088	0.41	.088	0.41	.088
1981	1.10	.489	1.10	.489	1.10	.489
1982	16.7	6.6	16.7	6.6	16.7	6.6
1983	46.9	23.7	44.1	22.7	44.9	23.0
1984	51.3	42.4	59.5	44.4	60.2	45.0
1985	59.2	64.0	68.0	69.2	67.1	69.5
1986	39.7	78.5	71.0	95.1	63.8	92.8
1987	30.1	89.5	73.0	121.9	59.0	114.3
1988	17.8	96.0	60.8	143.9	54.2	134.1
1989	11.5	100.2	46.6	160.9	50.1	152.4
1990	10.2	102.1	40.4	168.3	49.9	161.5
Extrapolated						
Ultimate Rec.		102.1		186.0		237.0

FORECAST, PRIMARY DEPLETION

Waskada Lower Amaranth Pool

RATE INJECTION/PRODUCTION SUMMARY:						

	INJECTION			PRODUCTION		
	GAS	WATER	OIL	POLYMER	AQUIFER	GAS
	m ³ /day	m ³ /day	m ³ /day	kg/day	m ³ /day	m ³ /day
TIME	PRESSURE					
Days	EPS					

[illegible]

FORECAST, WATER INJECTION

Waskada Lower Amaranth Pool

CUMULATIVE	INJECTION/PRODUCTION	SUMMARY:
DATE		
BY		
FOR		
REMARKS		

[illegible]

APPENDIX A

APPENDIX A

MODEL DEVELOPMENT AND DETAILED MODEL PREDICTIONS

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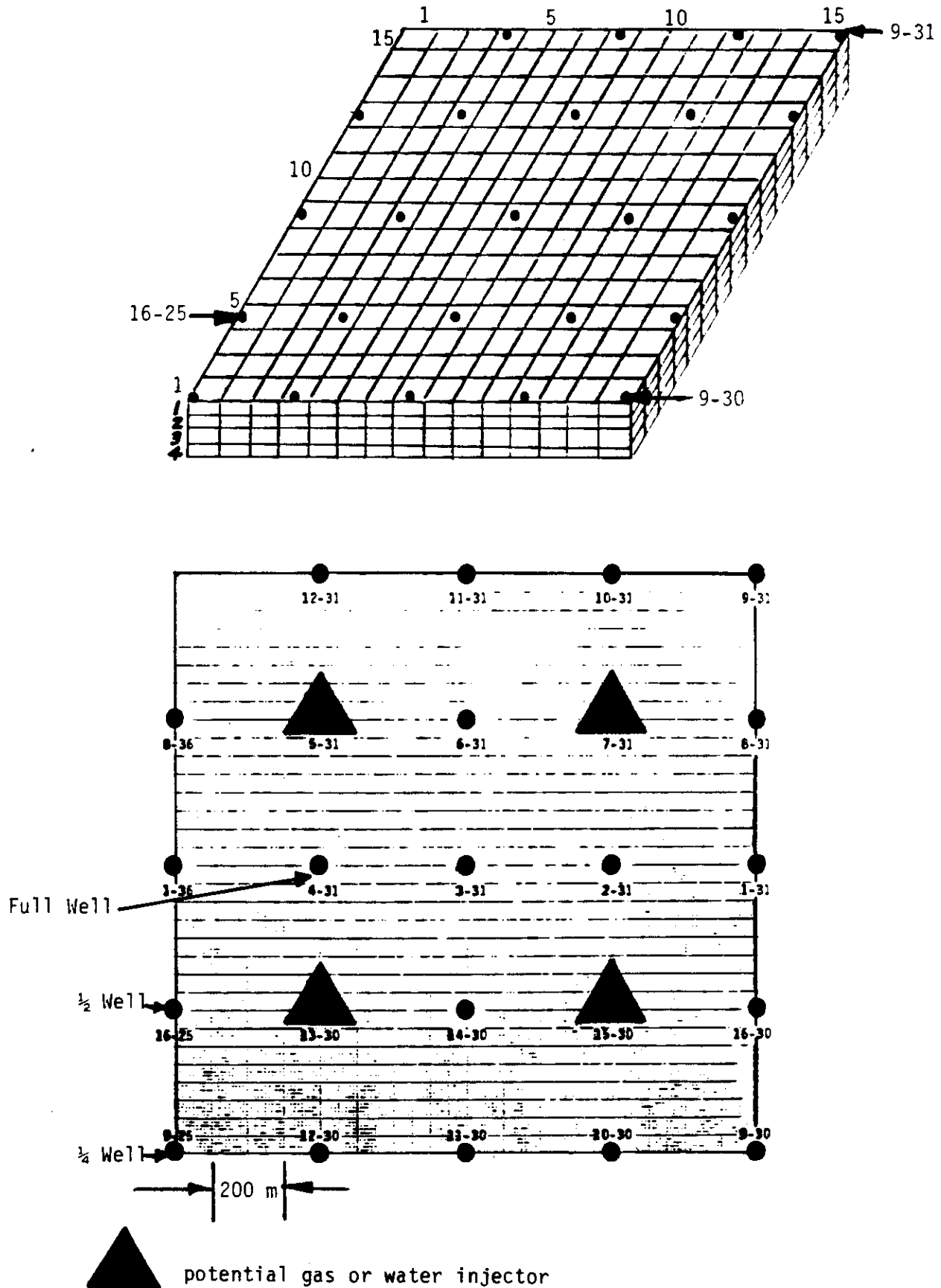
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Figure A-1

WELL LOCATIONS AND GRID BLOCK STRUCTURE FOR THE MODEL STUDY

Waskada Lower Amaranth Pool



C SAND STRUCTURE MAP

(Contour Interval = 0.5 m)

Waskada Lower Amaranth Pool

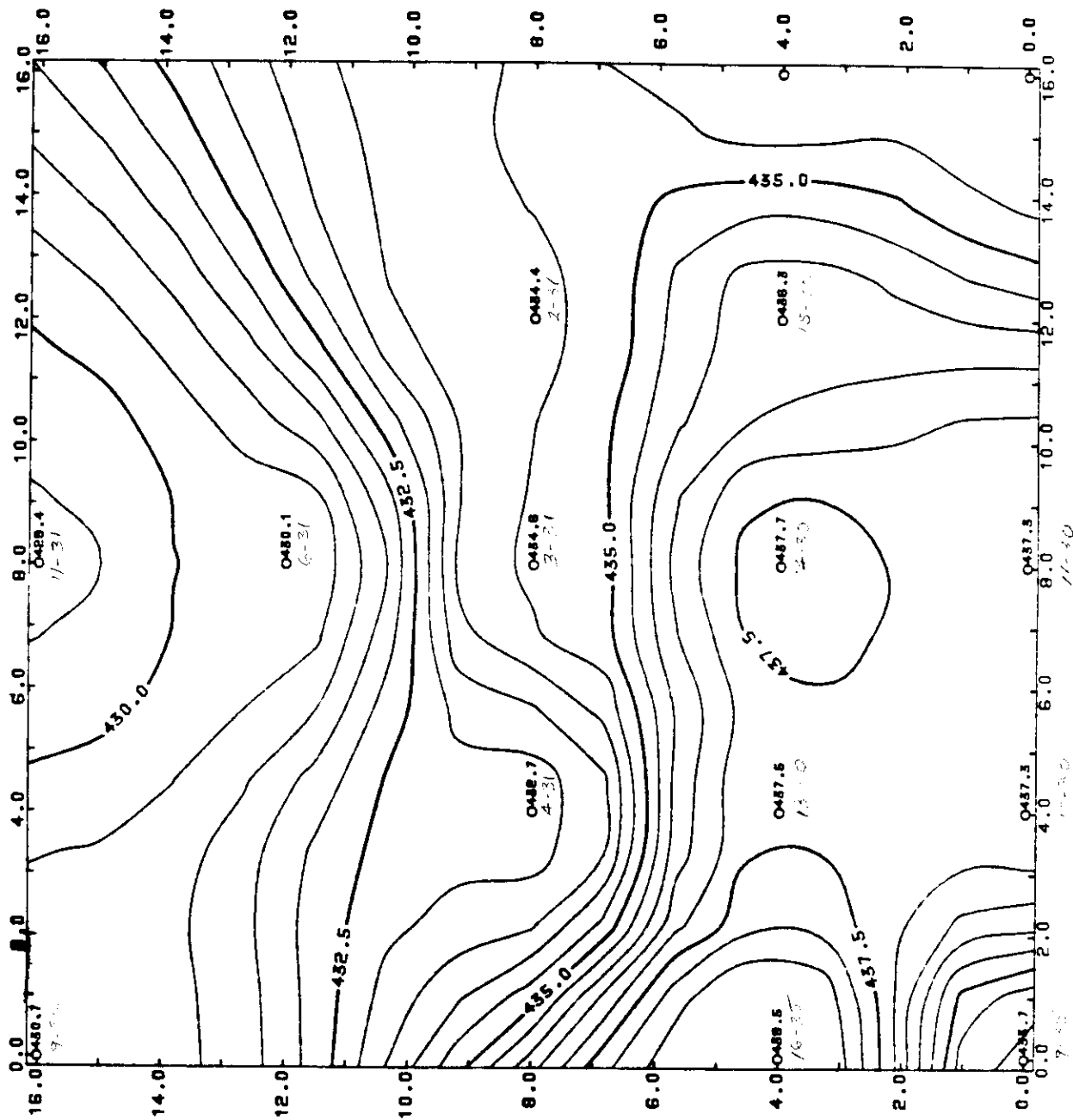


Figure A-3
 A SAND NET PAY CONTOUR MAP
 (Contour Interval = 0.1 m)
 Waskada Lower Amaranth Pool

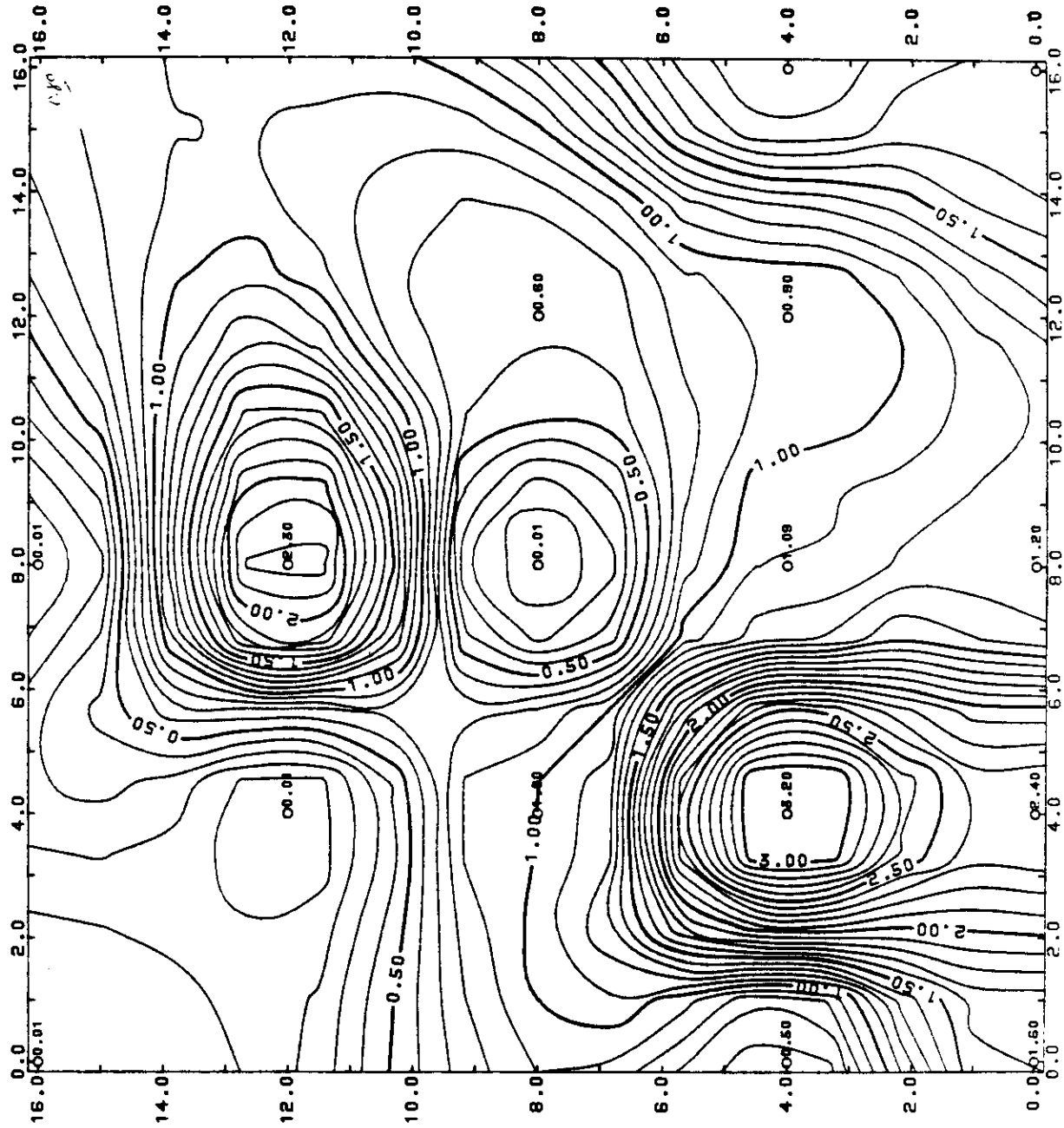


Figure A-4
B SAND NET PAY CONTOUR MAP
(Contour Interval = 0.2 m)
Waskada Lower Maranath Pool

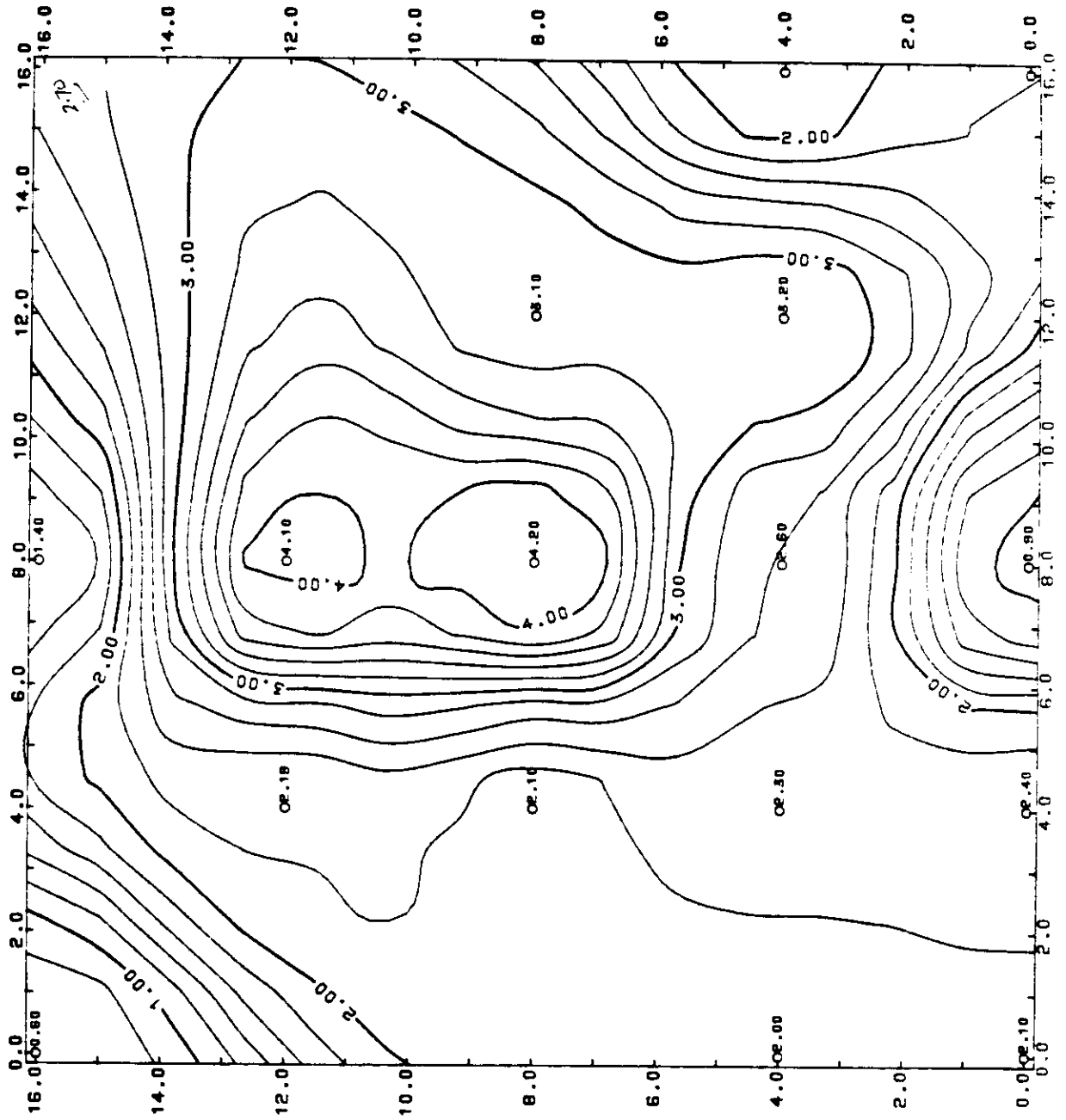


Figure A-5
 C SAND NET PAY CONTOUR MAP
 (Contour Interval = 0.2 m)
 Waskada Lower Amaranth Pool

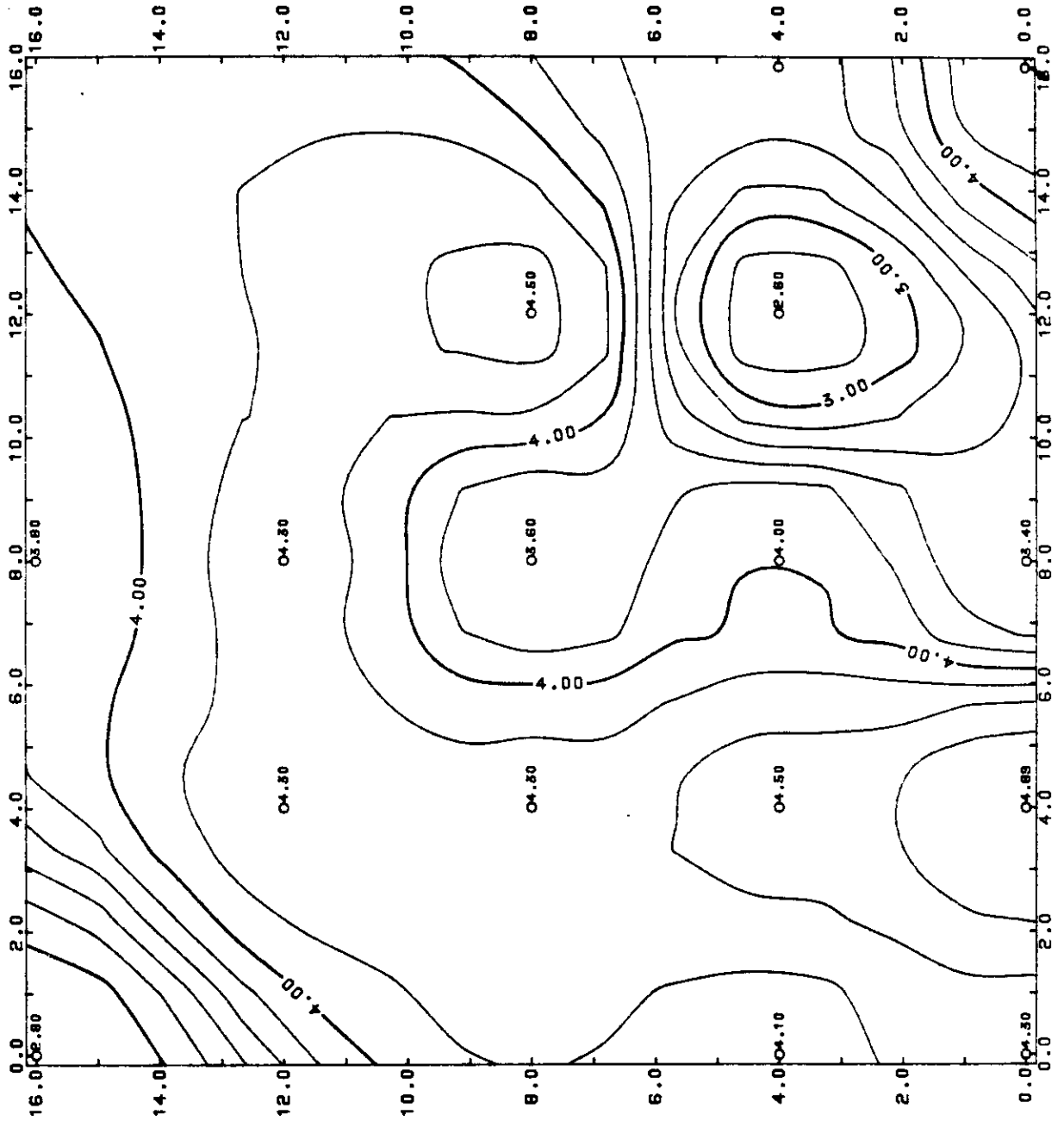


Figure A-6
 D SAND NET PAY CONTOUR MAP
 (Contour Interval = 0.2 m)
 Waskada Lower Amaranth Pool

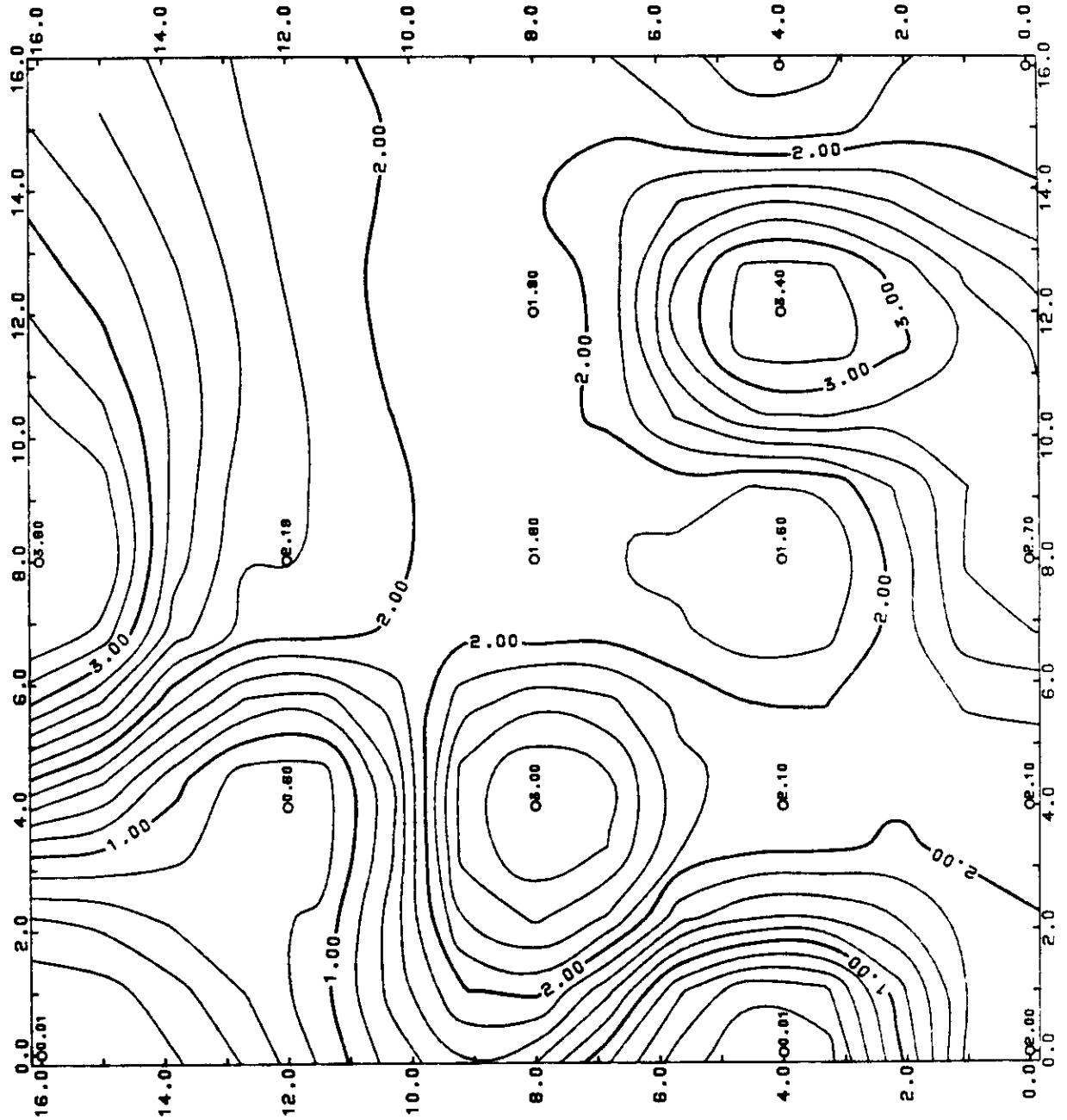


Figure A-7
 A SAND POROSITY CONTOUR MAP
 (Contour Interval = 0.01)
 Waskada Lower Amaranth Pool

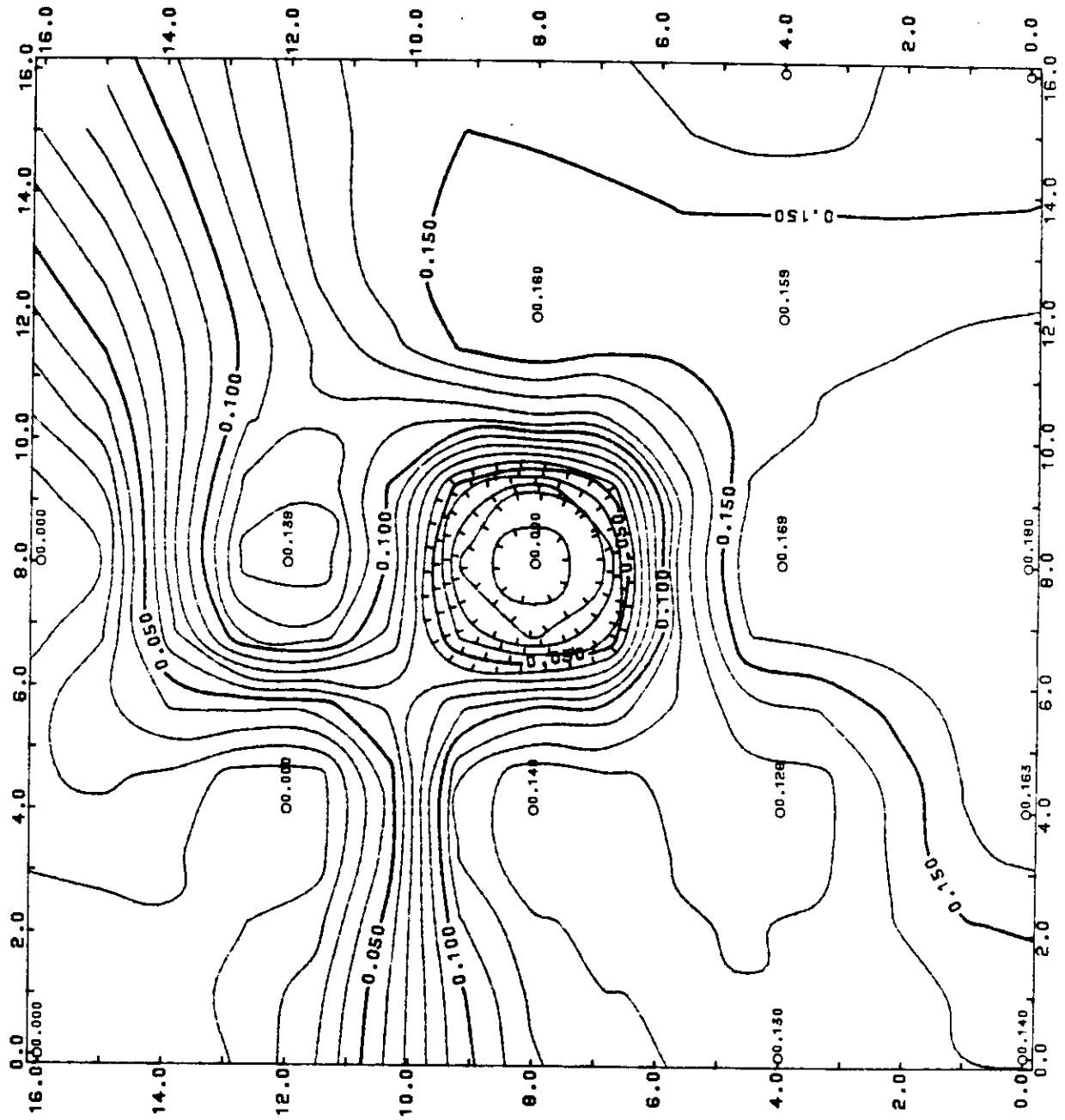


Figure A-8

B SAND POROSITY CONTOUR MAP

(Contour Interval = 0.01)

Waskada Lower Amaranth Pool

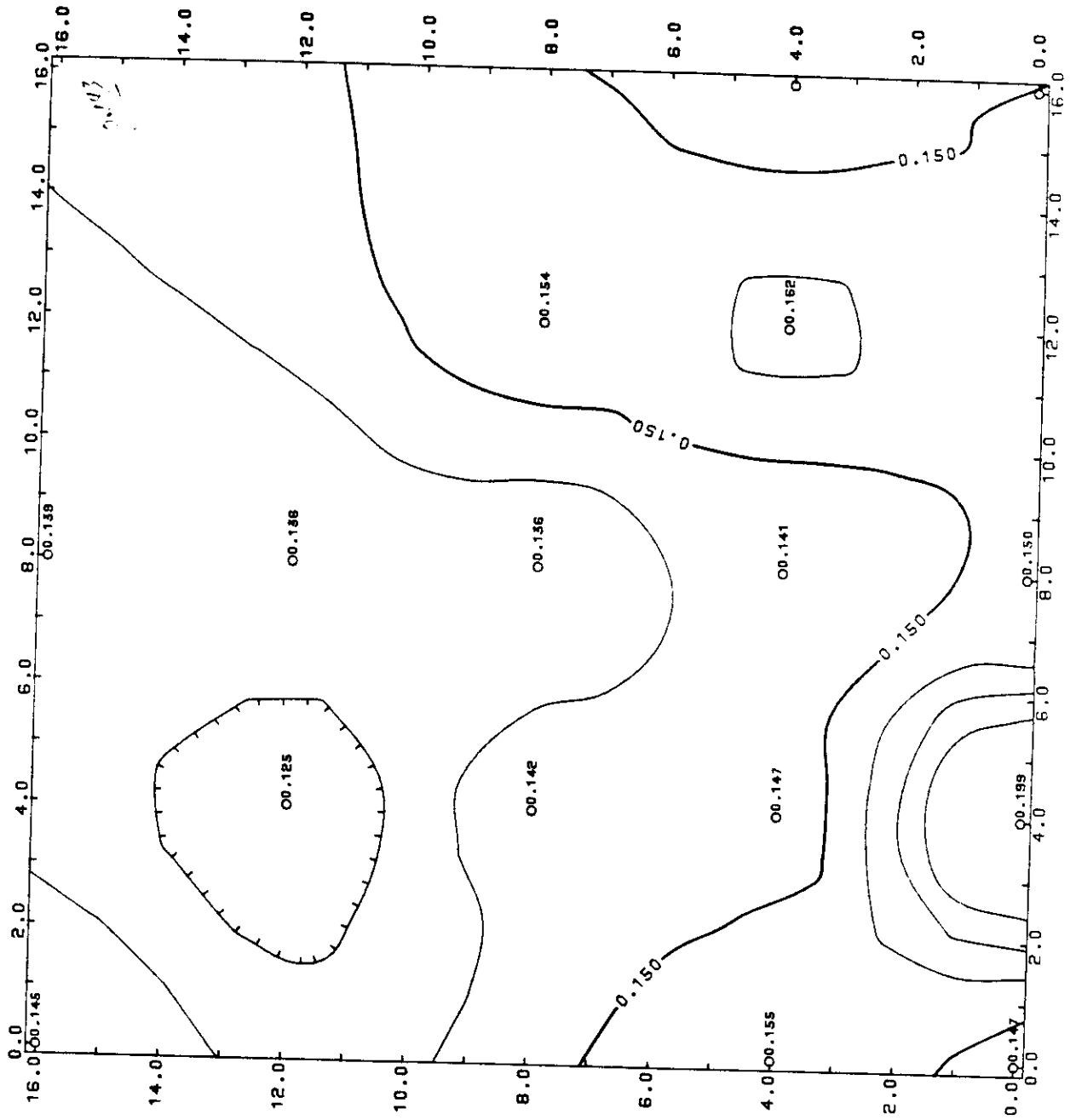


Figure A-9

C SAND POROSITY CONTOUR MAP

(Contour Interval = 0.01)

Maskada Lower Amaranth Pool

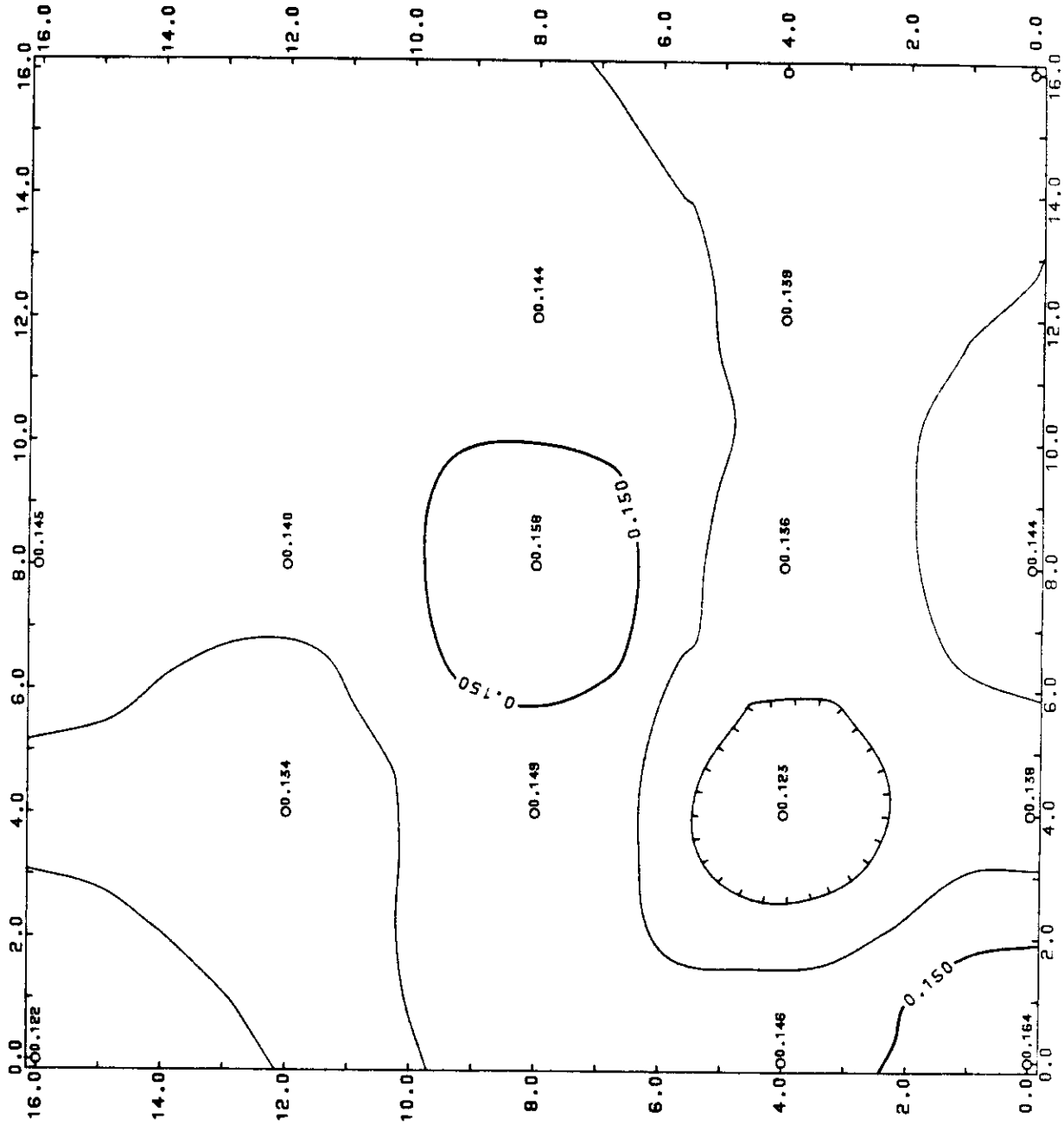


Figure A-10
 D SAND POROSITY CONTOUR MAP
 (Contour Interval = 0.01)
 Waskada Lower Amaranth Pool

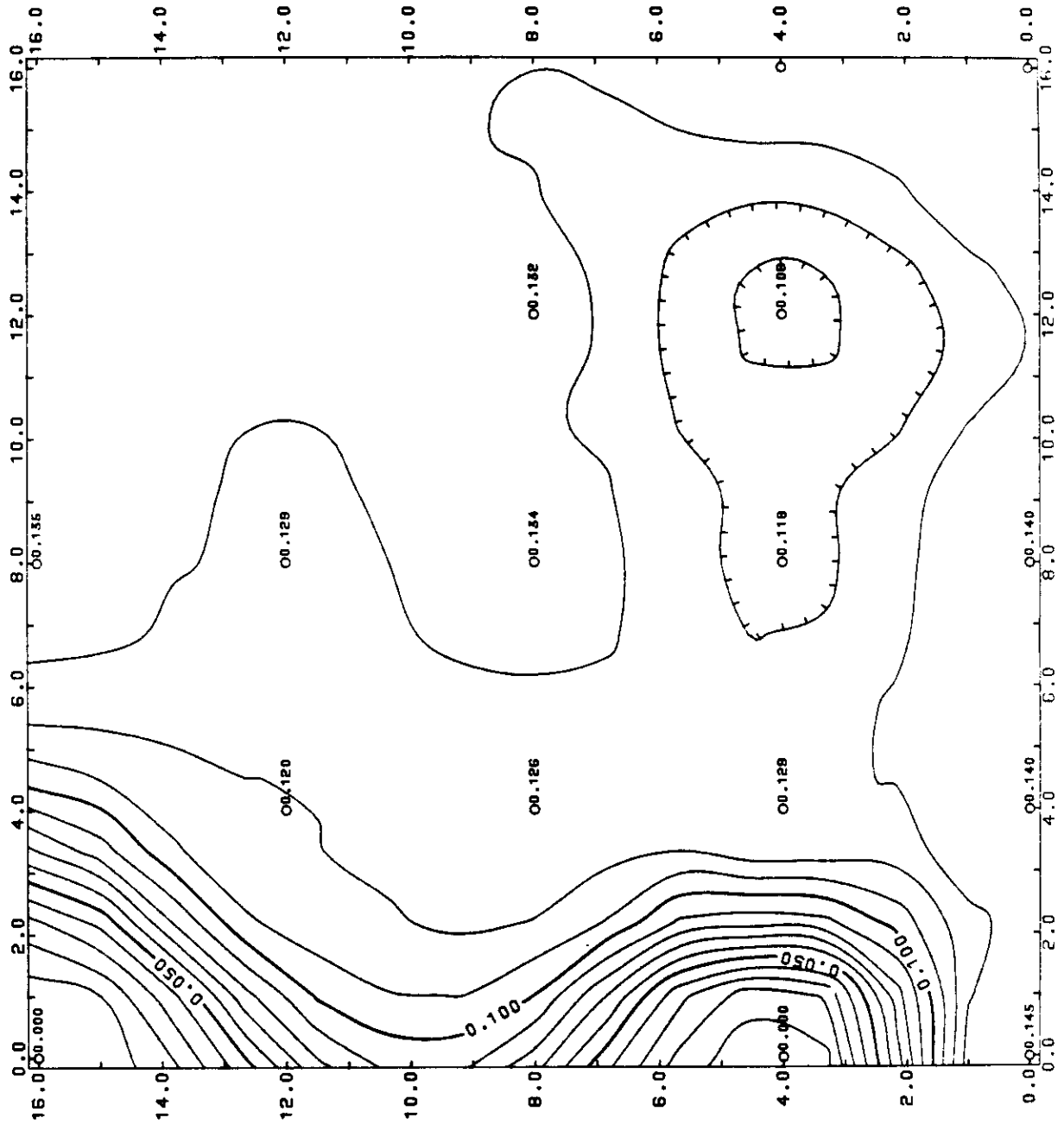


Figure A-11

PERMEABILITY VS POROSITY

Waskada Lower Amaranth Pool

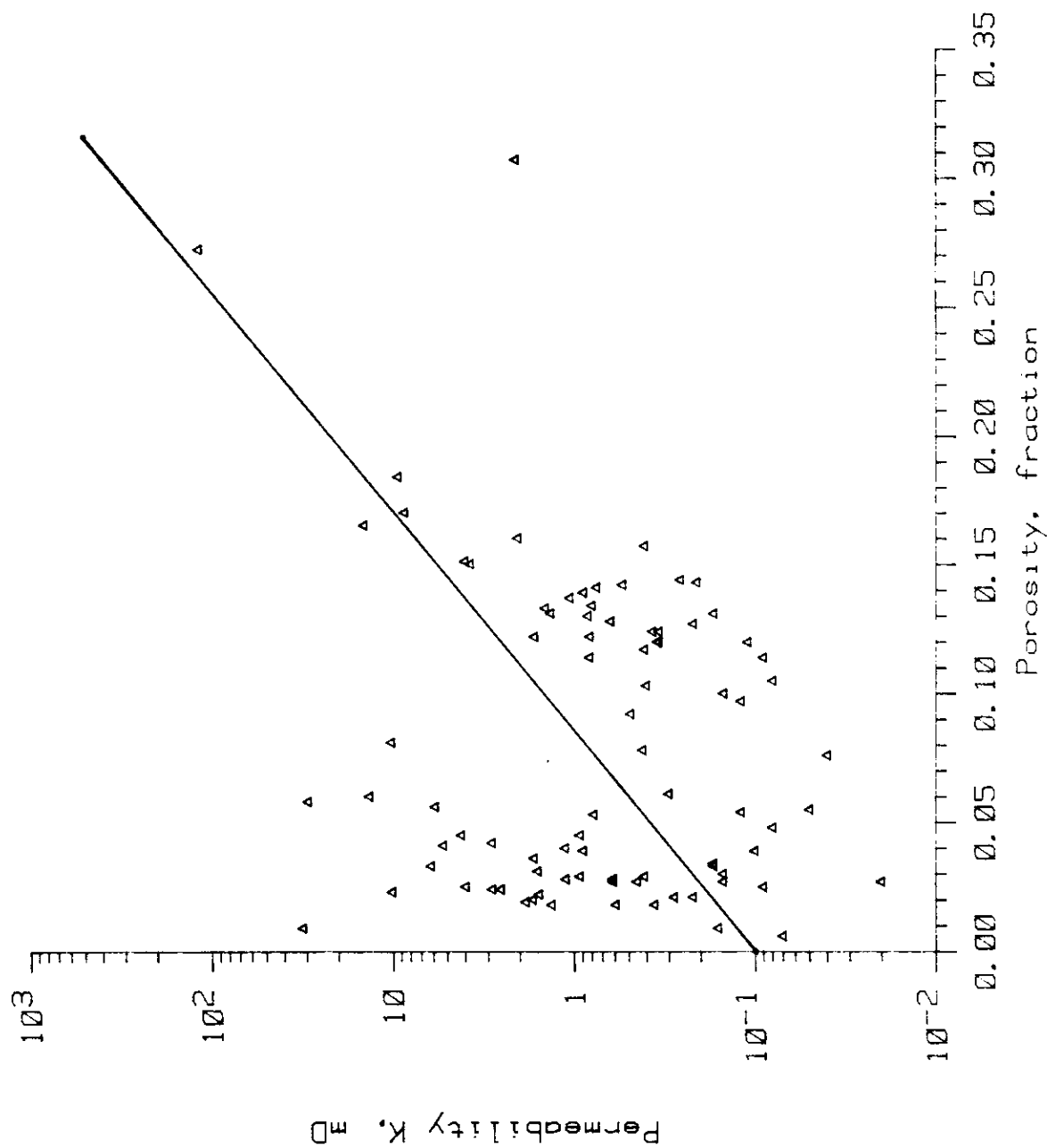


Figure A-12
OIL - WATER CAPILLARY PRESSURE
Waskada Lower Amaranth Pool

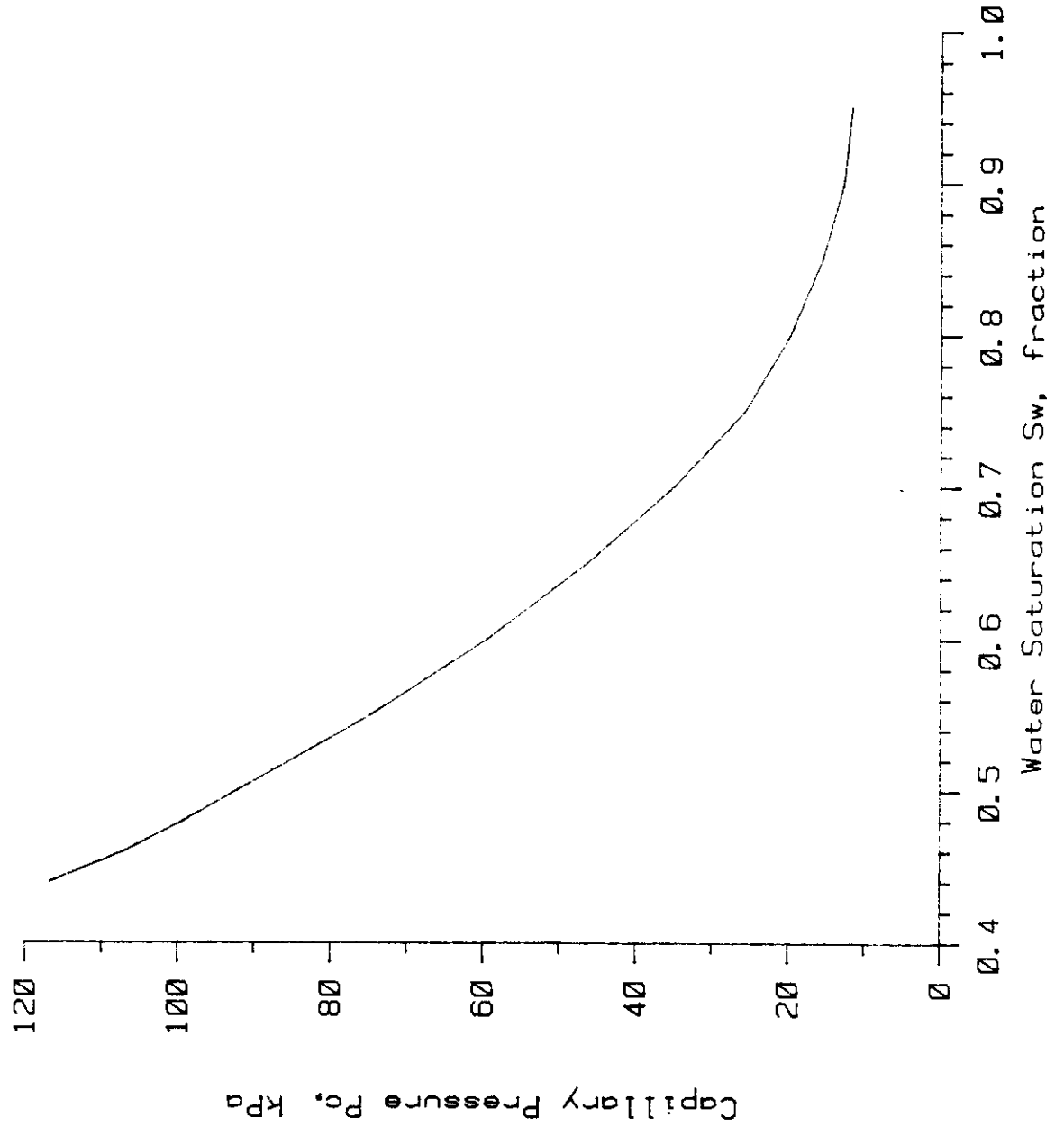


Figure A-13
OIL-WATER RELATIVE PERMEABILITY
Waskada Lower Amaranth Pool

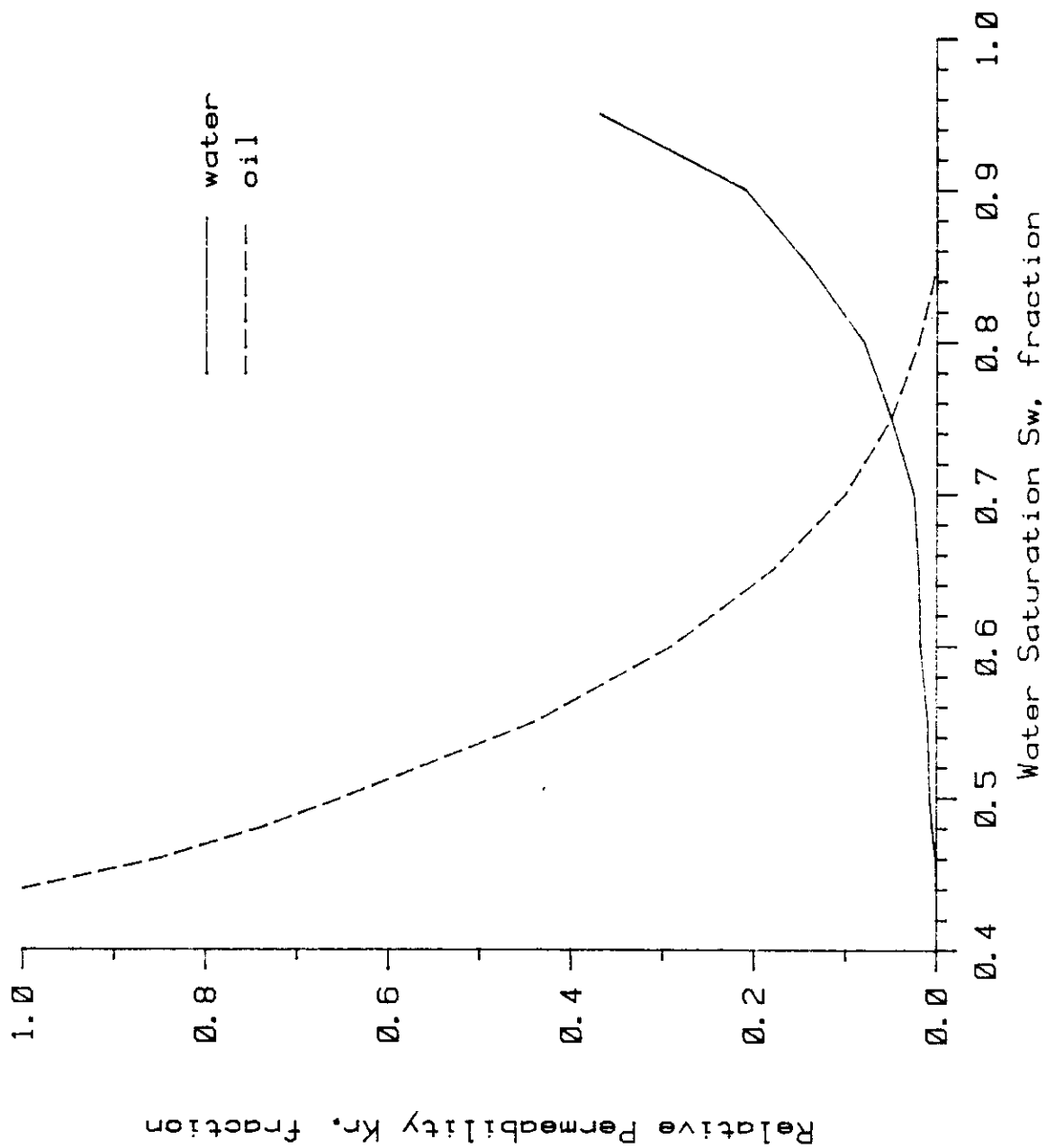


Figure A-14
GAS-OIL RELATIVE PERMEABILITY
Waskada Lower Amaranth Pool

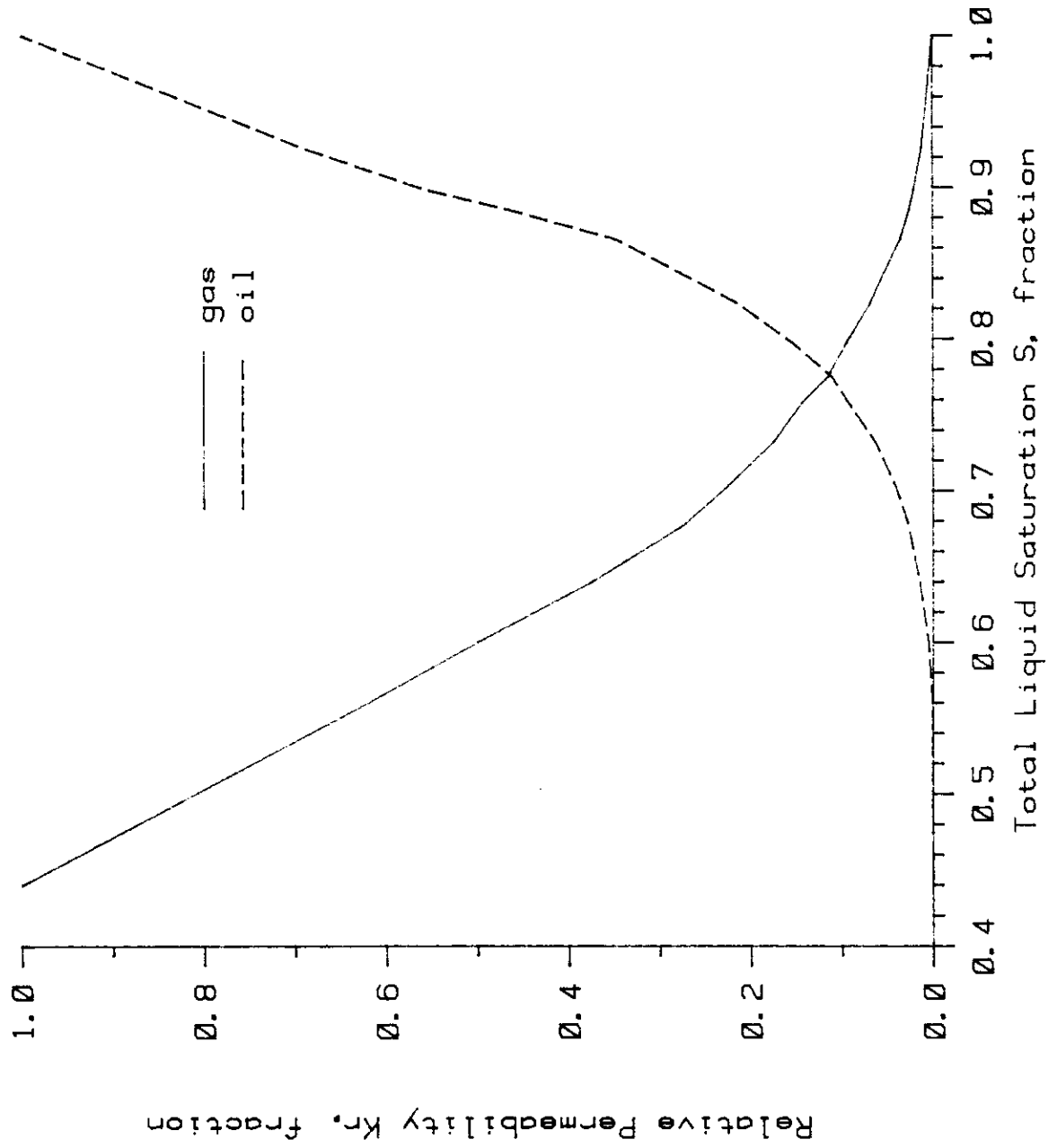


Table A-1
BLOCK CENTER DEPTH (RESERVOIR STRUCTURE)
Maskada Lower Amaranth Pool

time: 0.000 days

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Table A-1
BLOCK CENTER DEPTH (RESERVOIR STRUCTURE) (continued)
Waskada Lower Amaranth Pool

[illegible]

Waskada Lower Amaranth Pool.

plane 2 = 3

[illegible]

Table A-2
REFERENCE POROSITY (continued)
Waskada Lower Amaranth Pool

[illegible]

Table A-3

PERMEABILITY KX, mD

Maskada Lower Amaranth Pool

time: 0.000 days

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Table A-3
PERMEABILITY KX, MD (continued)
Waskada Lower Anaranth Pool

[illegible]

Table A-4

PERMEABILITY K^v , mD

Waskada Lower Amaranth Pool

time: 0-000 days

plane 201

plane 2a 2

3 June 1964

Table A-4
PERMEABILITY KY, mD (continued)
Waskada Lower Amaranth Pool

[illegible]

Table A-5
PERMEABILITY KZ, mD
Waskada Lower Anaranth Pool

time: 0.000 days

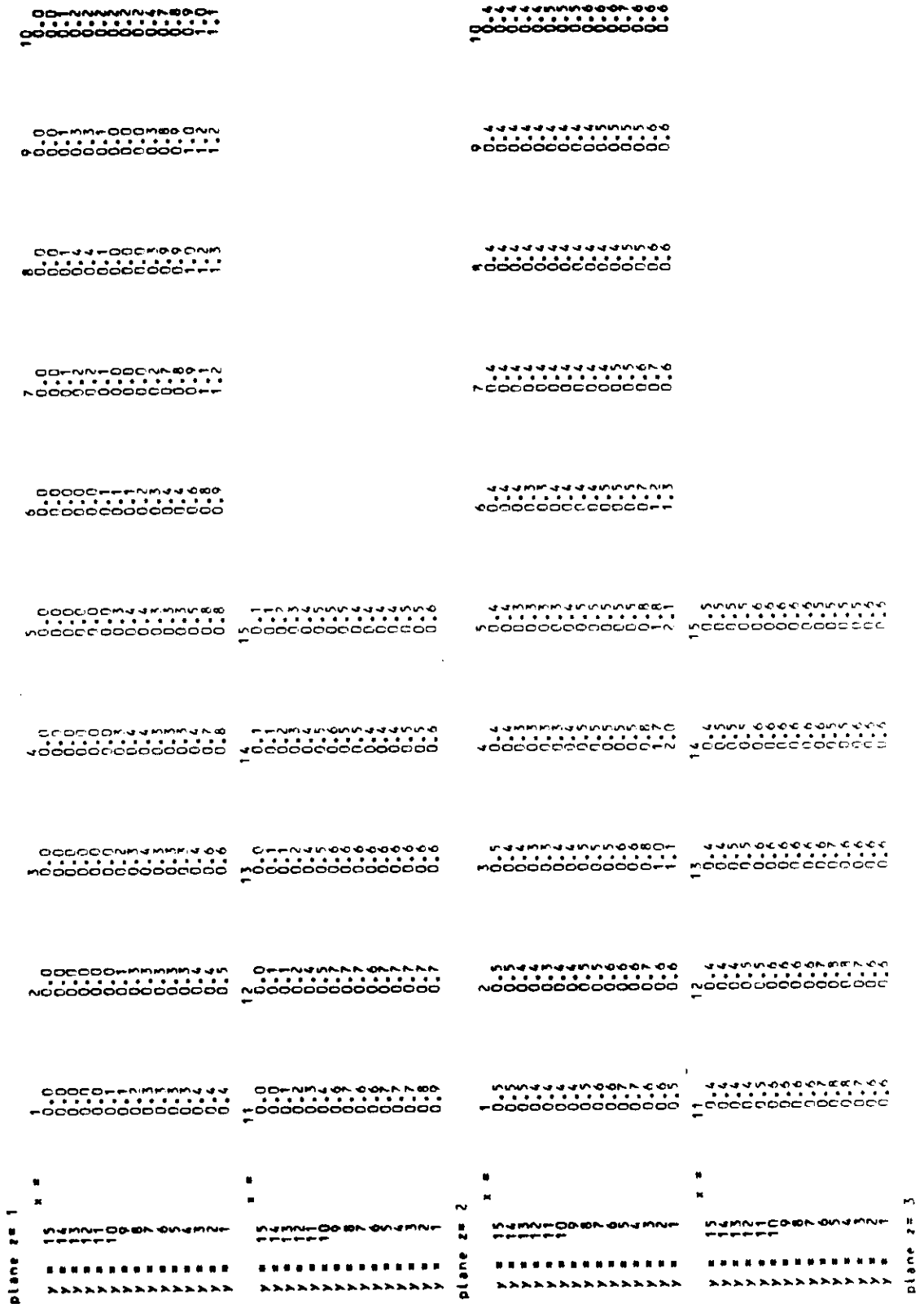


Table A-5
PERMEABILITY KZ, mD (continued)
Waskada Lower Amaranth Pool

[illegible]

Table A-7
INITIAL RESERVOIR PRESSURE (continued)
Waskada Lower Amaranth Pool

[illegible]

time: 0.000 days

<p> 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100 101 102 103 104 105 106 107 108 109 110 111 112 113 114 115 116 117 118 119 120 121 122 123 124 125 126 127 128 129 130 131 132 133 134 135 136 137 138 139 140 141 142 143 144 145 146 147 148 149 150 151 152 153 154 155 156 157 158 159 160 161 162 163 164 165 166 167 168 169 170 171 172 173 174 175 176 177 178 179 180 181 182 183 184 185 186 187 188 189 190 191 192 193 194 195 196 197 198 199 200 201 202 203 204 205 206 207 208 209 210 211 212 213 214 215 216 217 218 219 220 221 222 223 224 225 226 227 228 229 230 231 232 233 234 235 236 237 238 239 240 241 242 243 244 245 246 247 248 249 250 251 252 253 254 255 256 257 258 259 260 261 262 263 264 265 266 267 268 269 270 271 272 273 274 275 276 277 278 279 280 281 282 283 284 285 286 287 288 289 290 291 292 293 294 295 296 297 298 299 300 301 302 303 304 305 306 307 308 309 310 311 312 313 314 315 316 317 318 319 320 321 322 323 324 325 326 327 328 329 330 331 332 333 334 335 336 337 338 339 340 341 342 343 344 345 346 347 348 349 350 351 352 353 354 355 356 357 358 359 360 361 362 363 364 365 366 367 368 369 370 371 372 373 374 375 376 377 378 379 380 381 382 383 384 385 386 387 388 389 390 391 392 393 394 395 396 397 398 399 400 401 402 403 404 405 406 407 408 409 410 411 412 413 414 415 416 417 418 419 420 421 422 423 424 425 426 427 428 429 430 431 432 433 434 435 436 437 438 439 440 441 442 443 444 445 446 447 448 449 450 451 452 453 454 455 456 457 458 459 460 461 462 463 464 465 466 467 468 469 470 471 472 473 474 475 476 477 478 479 480 481 482 483 484 485 486 487 488 489 490 491 492 493 494 495 496 497 498 499 500 501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518 519 520 521 522 523 524</p>
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Table A-8

[illegible]

Table A-9
INITIAL WATER SATURATION (continued)
Waskada Lower Amaranth Pool

[illegible]

Table A-10

PVT FUNCTIONS

Waskada Lower Amaranth Pool

PVT FUNCTIONS									
Pressure kPa	Sol'n gas m ³ /m ³	Oil vol m ³ /m ³	Gas vol m ³ /m ³	Gas exp m ³ /m ³	Oil visc cP	Gas visc cP			
0.000	0.200	1.02502	1.00000	1.000	2.006	0.01020			
958.000	20.350	1.02507	0.10343	9.650	2.006	0.01040			
1413.000	34.540	1.02513	0.07179	15.930	1.212	0.01080			
2082.000	39.540	1.02520	0.04324	20.230	1.212	0.01130			
2683.000	42.200	1.02520	0.03658	27.340	1.219	0.01150			
3482.000	47.600	1.02500	0.02963	33.750	1.285	0.01190			
4220.000	51.040	1.02003	0.02488	40.200	1.500	0.01280			
4895.000	61.500	1.01803	0.01543	64.800	1.540	0.01400			
10342.000	81.500	1.00803	0.01146	95.600	1.540	0.01400			

Table A-11
 SEQUENTIAL DEVELOPMENT
 Waskada Lower Amaranth Pool

<u>Date</u>	<u>Total Number of Wells on Production</u>	<u>Well Names</u>
80-06-02	1	11-30
80-12-02	0	---
81-01-02	1	11-30
82-02-15	2	Previous well plus: 9-25.
82-03-04	4	Previous wells plus: 9-30, 3-31.
82-08-13	5	Previous wells plus: 4-31.
82-08-27	6	Previous wells plus: 13-30.
82-09-11	7	Previous wells plus: 14-30.
82-09-14	8	Previous wells plus: 6-31.
82-09-16	10	Previous wells plus: 15-30, 16-30.
82-10-15	11	Previous wells plus: 2-31.
82-10-25	12	Previous wells plus: 16-25.
82-12-18	13	Previous wells plus: 11-31.
83-10-02	20	Previous wells plus: 1-31, 5-31, 7-31, 8-31 9-31, 10-31, 12-31.
84-10-02	24	Previous wells plus: 10-30, 12-30, 1-36, 8-36.

Table A-12

TEN-YEAR RECOVERY BY WELLS

Waskada Lower Amaranth Pool

Well No.	Well Name	Recovery, m ³			Well Type
		Primary	Gas Inj.	Water Inj.	
1	9-30	486.9	1 341.2	1.341.2	1/4
2	10-30	2 119.3	4 961.6	4 995.2	1/2
3	11-30	857.8	1 759.6	1 759.6	1/2
4	12-30	2 002.1	3 270.4	4 761.7	1/2
5	13-30	3 062.9	661.6*	661.6**	1
6	14-30	6 521.1	13 164.4	11 394.4	1
7	15-30	4 731.6	1 382.6*	1 382.6**	1
8	16-30	3 889.6	5 979.6	5 985.3	1/2
9	1-31	2 466.7	5 516.6	5 528.4	1/2
10	2-31	10 988.8	21 398.4	19 268.3	1
11	3-31	5 274.5	8 904.2	8 904.2	1
12	4-31	8 933.4	16 207.3	14 596.8	1
13	5-31	4 950.1	-- *	-- **	1
14	6-31	12 315.7	19 613.4	20 039.8	1
15	7-31	7 256.8	-- *	-- **	1
16	8-31	3 139.0	5 459.5	5 514.9	1/2
17	9-31	1 848.0	7 057.2	7 177.7	1/4
18	10-31	3 311.5	8 009.7	7 834.5	1/2
19	11-31	5 931.2	14 767.9	12 588.4	1/2
20	12-31	2 503.0	5 125.0	5 173.8	1/2
21	9-25	2 600.3	7 292.3	7 183.8	1/4
22	16-25	3 859.2	6 691.5	6 756.9	1/2
23	1-36	1 552.7	5 427.2	4 358.1	1/2
24	8-36	1 523.4	4 303.8	4 287.3	1/2
TOTAL		102 125.6	168 295.0	161 494.5	

*Converted to gas injectors

**Converted to water injectors

Table A-13

[illegible]

[illegible][illegible][illegible]

.....

[illegible][illegible][illegible][illegible][illegible][illegible]

Table A-13

Table A-14

[illegible]

[illegible]

times 3650,000 days

[illegible]

[illegible]

Table A-16
GAS INJECTION - RUN TIME SUMMARY (continued)
Waskada Lower Amaranth Pool

501
111
137
259
358
915

17-1

Table A-16
GAS INJECTION - RUN TIME SUMMARY (continued)
Waskada Lower Amaranth Pool

[illegible]

[illegible]

[illegible]

Table A-17

GAS INJECTION - CUMULATIVE INJECTION/PRODUCTION SUMMARY (continued)

Waskada Lower Amaranth Pool

[illegible]

Table A-18
GAS INJECTION - OIL SATURATION AT THE END OF THE FORECAST
Waskada Lower Anaranth Pool

[illegible]

[illegible]

WATER INJECTION - RUN TIME SUMMARY

Waskada Lower Amaranth Pool

[illegible]

Waskada Lower Amaranth Pool

[illegible]

[illegible]

[illegible]

Table A-21
WATER INJECTION - OIL SATURATION AT THE END OF THE FORECAST
Waskada Lower Amaranth Pool

[illegible]

Alaskada Lower Amaranth Pool

[illegible]

APPENDIX B

APPENDIX B

FLUID DISTRIBUTION CURVES AND HISTORY MATCH RESULTS

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APPENDIX B

Development of Fluid Distribution Curves.

To develop this set of curves the following steps are required:

. Convert the laboratory initial displacement pressure, observed in the laboratory capillary pressure curve, to equivalent reservoir initial displacement pressure. The relevant expression is given by

$$(P_C)_R = (P_C)_L * \frac{(\gamma_{ow})_R}{(\gamma_{ow})_L}$$

where

$(P_C)_R$	is the reservoir capillary pressure
$(P_C)_L$	is the laboratory capillary pressure
$(\gamma_{ow})_R$	is the interfacial tension of the reservoir fluid system, i.e. oil-water (= 28 dynes/cm)
$(\gamma_{ow})_L$	is the interfacial tension of the laboratory fluid system, i.e. air-water (= 72 dynes/cm)

Using the laboratory capillary pressure data, the reservoir capillary pressure for the observed initial laboratory displacement pressure is calculated as follows:

$$(P_C)_R = 4.35 \text{ psi} \times \frac{28}{72} = 1.69 \text{ psi}$$

. Convert the reservoir capillary pressure to height using the following expression:

$$h_{ID} = \frac{144 (P_C)_R}{(\rho_w - \rho_o)}$$

or

$$h_{ID} = \frac{144 \times 1.69}{(63.5 - 40.8) \text{ lb/ft}^3} = 10.7 \text{ ft} = 3.3 \text{ m}$$

. Calculate the free water level (FWL) or zero capillary pressure level to have the same initial conditions as in the laboratory.

$$FWL = -IOWC - 3.3$$

where IOWC is the estimated initial field oil-water contact, i.e. -465 m subsea. Therefore,

$$FWL = -465 - 3.3 = -468.3 \text{ m}$$

. Determine a relationship between depth and laboratory capillary pressure as shown in Figure B-1. This is done using the following expression:

$$(P_c)_R = \frac{h (\rho_w - \rho_o)}{144}, \quad h = FWL - \text{Depth subsea}$$

and

$$(P_c)_L = (P_c)_R \times \frac{(\gamma_{aw})_L}{(\gamma_{ow})_R}$$

. Plot the laboratory capillary pressure for different core permeabilities to obtain the fluid distribution curves shown in Figure B-2.

Procedure to Calculate Water Saturation

- . Locate the depth of interest in Figure B-1 and read the corresponding laboratory capillary pressure.
- . Using the porosity value, determine the expected permeability applying the best available porosity-permeability relationship.
- . Identify in Figure B-2 the capillary pressure curve to be used for the required interval in the well. Each individual permeability value should be close to one of the curves shown in Figure B-2.
- . Using the laboratory capillary pressure obtained from Figure B-1 for each subsea depth and the corresponding permeability value, the water saturation for each interval is obtained directly from the fluid distribution curves, Figure B-2.

The tabular set up would be as follows:

<u>Subsea Depth, m</u>	<u>$(P_c)_L$, kPa</u>	<u>Curve No. (Figure B-2)</u>	<u>Water Saturation, %</u>
-	-	-	-
-	-	-	-
-	-	-	-

Calculation of Flowing Bottom Hole Pressures

A series of fluid level and well rate tests were conducted on wells 9-30, 13-30, 14-30, 15-30, 16-30, 9-25, 16-25, 2-31, 3-31, 4-31, 6-31, and 11-31 as shown in Table C-1.

B

To calculate flowing bottom hole pressures, the following procedure is used: (Calculations are shown for well 9-30)

- . from Table C-1, read fluid level (oil column), i.e. oil column = 940 m = 3080 ft.
- . from Table C-1, read oil and water rates
oil rate = 1.24 m³/d
water rate = 0.25 m³/d
- . calculate water cut on 83-01-12

$$f_w = \frac{0.25}{0.25 + 1.24} = .17 = 17\%. \text{ This water cut is very much}$$

different from the 48.2% corresponding to the 1982 average. This suggests a somewhat erratic production data for this initial period. Similar differences were calculated for the other wells.

- . calculate average pressure gradient ρ_{avg}

$$\rho_{avg} = \frac{1.24 \times 0.28 + 0.25 \times 0.433}{1.24 + 0.25} = .305 \text{ psi/ft}$$

With a bottom hole depth of 3080 ft, flowing bottom hole pressure
 = 3080 x 0.305
 = 939 psi
 = 6479 kPa

History Match Results

Table B-2 shows the history match of water-cut and flowing bottomhole pressures for twelve wells currently drilled in the model area (no data was taken in the 11-30 well). Considering the somewhat erratic initial production data for the water-cut measurements, which are also required in calculating the average fluid gradient, the match shown in Table B-2 was considered satisfactory.

To get a history match the following procedure was followed:

- all wells in the model were fractured to increase their flow capacity and to provide a reasonable level of flowing bottomhole pressures. This simulated the actual fracturing of the wells in the field. Fracturing in the model was performed by multiplying by a factor of 10 or 30, the permeabilities of the grid blocks containing well elements, and their corresponding adjacent grid blocks.
- the water relative permeability curve was adjusted to bring predicted water cuts more closely in line with the observed distribution of water-cut values.

Figure B-1
DEPTH VS LABORATORY CAPILLARY PRESSURE
Waskada Lower Amaranth Pool

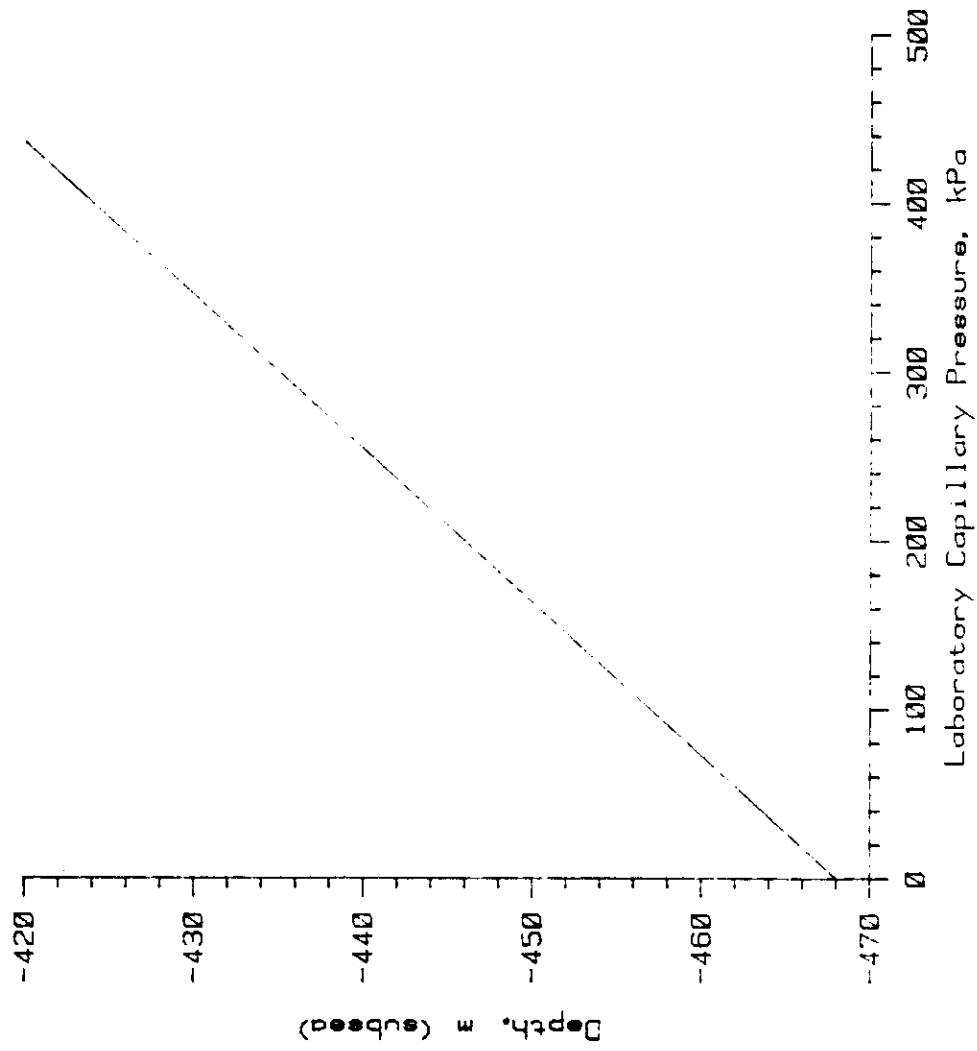


Figure B-2

FLUID DISTRIBUTION CURVES

Waskada Lower Amaranth Pool

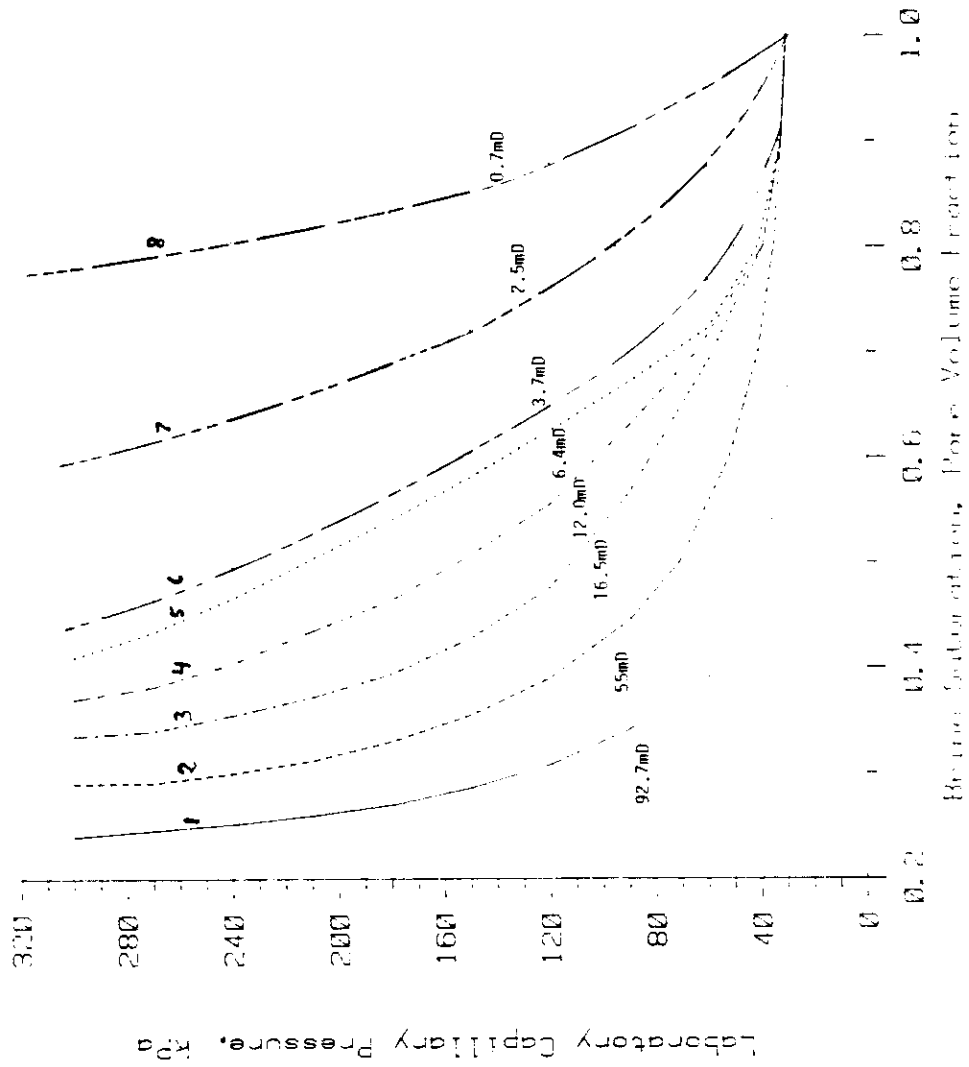


Table B-1

FLUID LEVELS AND WELL TEST RESULTS

Waskada Lower Amaranth Pool

Well Location	Fluid Level (m)	Date	Test Results				
			Oil (m ³)	Water (m ³)	Gas (km ³)	Hours	Date
9-30-1-25 W1M	940	83-01-12	1.24	0.25	N/A	24	83-01-12
13-30	585	83-01-11	7.94	1.98	0.30	24	83-01-02
14-30	350	83-01-11	7.95	2.65	0.30	24	83-01-03
15-30	192	83-01-12	2.50	4.09	0.04	24	83-01-06
16-30	532	83-01-12	4.11	4.11	0.15	23½	83-01-05
9-25-1-26	912	83-01-11	0.38	0.21	0.05	24	81-01-04
16-25	917	83-01-11	0.98	0.05	0.22	24	83-12-22
2-31-1-25	250	83-01-15	N/A	N/A	N/A	N/A	N/A
3-31	922	83-01-15	N/A	N/A	N/A	N/A	N/A
4-31	922	83-01-12	N/A	N/A	N/A	N/A	N/A
6-31	269	83-01-15	N/A	N/A	N/A	N/A	N/A
11-31	355	83-01-15	N/A	N/A	N/A	N/A	N/A

Table B-2

HISTORY MATCH RESULTS

Waskada Lower Amaranth Pool

Well	Field Measurements		Model Predictions	
	Water Cut, % (1982 average)	Flowing Bottom Hole Pressure, kPa (83-01-12)	Water Cut, % (83-01-14)	Flowing Bottom Hole Pressure, kPa (83-01-14)
9-30	48.2	6479	33.1	5414
11-30	50.0	N/A	66.6	4321
13-30	78.0	4106	66.6	3563
14-30	38.0	2520	64.9	2542
15-30	31.0	1630	47.8	1438
16-30	46.0	4350	40.3	3902
2-31	33.0	N/A	44.0	2413
3-31	50.0	N/A	43.4	4646
4-31	30.0	N/A	39.1	3112
6-31	30.0	N/A	21.1	4620
9-25	9.6	7014	46.0	3626
16-25	36.0	5840	78.1	500